

Multigrid acceleration of a preconditioned Krylov method for the solution of the discretized vector wave equation

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 - Krylov subspace method for the preconditioner system
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NLR

- NLR = Nationaal Lucht- en Ruimtevaartlaboratorium (in Dutch)
National Aerospace Laboratory (in English)
- Consists of two residences: one in Amsterdam and one in NOP¹, Marknesse
- Independent technological institute
- About 700 employees

¹NOP = Noordoostpolder

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Problem description

- When the radar signature of a military platform cannot be determined experimentally, *numerical prediction* techniques are used
- In this thesis a faster and more memory efficient prediction method is proposed

- **RADAR (Radio Detection and Ranging):** technology to detect military platforms (e.g. aircraft, ship or tank) by using electromagnetic waves

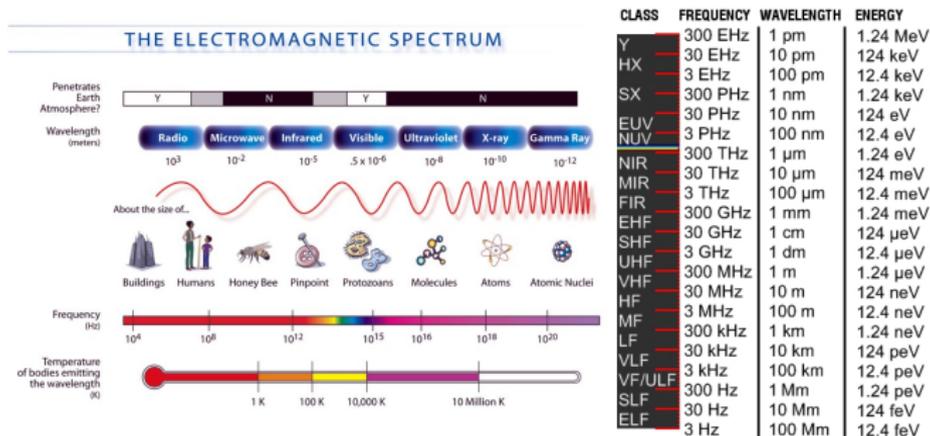


Figure: RADAR – infrared detection – optic detection

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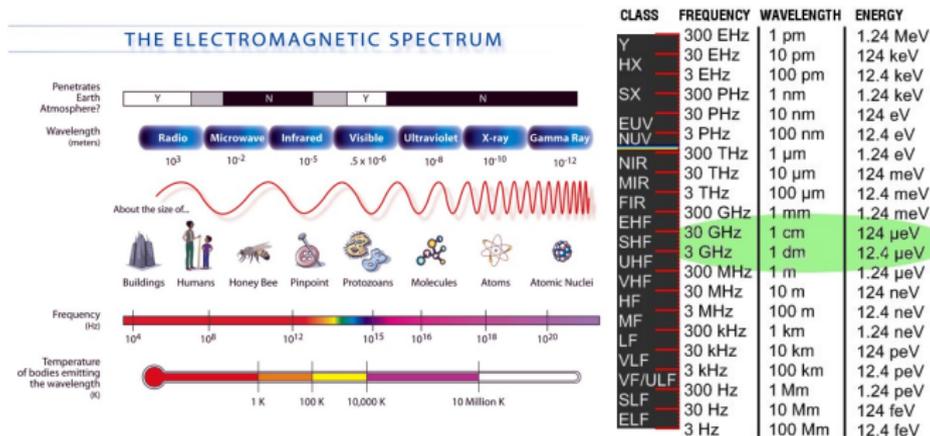


Figure: RADAR – infrared detection – optic detection

Assumptions – mathematical model

- Radar excited from the front: jet engine air intake (of a modern fighter aircraft) accounts for the major part of the RCS for a large range of observation angles
- Maxwell's equations \Rightarrow vector wave equation

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Figure: Jet engine air intake (left) closed by jet engine compressor fan (right) – together forms a **large and deep open-ended cavity** with varying cross section – *Dimensions: $d \approx 30\lambda$ and $L \approx 200\lambda$ for X-band excitation (10 GHz)*



RCS – definition

- Measure of detectability: **radar cross section (RCS)**
(depends on observation angle, frequency, polarization)
- A platform is detected when the signal-to-noise ratio exceeds a certain threshold

RCS: measure or predict?

Measuring RCS not possible if:

- platform is still in design, development or procurement phase or belongs to a hostile party
- time consuming or measurements too expensive
⇒ **Numerical prediction techniques must be used**

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$$\begin{aligned}\nabla^* \times \mathcal{E}^* &= -\frac{\partial^* \mathcal{B}^*}{\partial^* t^*} \\ \nabla^* \times \mathcal{H}^* &= \frac{\partial^* \mathcal{D}^*}{\partial^* t^*} + \mathcal{J}^* \\ \nabla^* \cdot \mathcal{D}^* &= \mathcal{Q}^* \\ \nabla^* \cdot \mathcal{B}^* &= 0 \\ \nabla^* \cdot \mathcal{J}^* &= -\frac{\partial^* \mathcal{Q}^*}{\partial^* t^*}\end{aligned}$$

The following (dimension full) variables are used with their S.I. unit between brackets:

\mathcal{E}^* = electric field intensity [$\frac{V}{m}$]

\mathcal{D}^* = electric flux density [$\frac{C}{m^2}$]

\mathcal{H}^* = magnetic field intensity [$\frac{A}{m}$]

\mathcal{B}^* = magnetic flux density [$\frac{Wb}{m^2}$]

\mathcal{J}^* = electric current density [$\frac{A}{m^2}$]

\mathcal{Q}^* = electric charge density [$\frac{C}{m^3}$]

t^* = time [s]

The vector wave equation (1/2)

Under additional assumptions:

field quantities above are harmonic oscillating functions with an angular frequency ω^* (*time-harmonic functions*)

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The vector wave equation (1/2)

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Maxwell's equations are rewritten in *phasor* quantities as:

$$\nabla^* \times \mathbf{E}^* = j\omega^* \mathbf{B}^*$$

$$\nabla^* \times \mathbf{H}^* = j\omega^* \mathbf{D}^* + \mathbf{J}^*$$

$$\nabla^* \cdot \mathbf{J}^* = -j\omega^* q^* \qquad j^2 = -1$$

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The vector wave equation (2/2)

Combined with the *constitutive relations*², the dimensionless *vector wave equation* for the electric field can be derived as:

$$\nabla \times \nabla \times \mathbf{E} - k_0^2 \mathbf{E} = -jk_0 Z_0 \mathbf{J} \quad (1)$$

Additional boundary conditions to obtain a well-posed problem:

$$\begin{aligned} (\hat{n} \times \mathbf{E})_{S_{\text{mantle}}} &= 0 \\ (\hat{n} \times \mathbf{H}^{\text{inc}})_{S_{\text{aperture}}} &= 4\hat{n} \times \left\{ \frac{\nabla^2 \cdot \mathbf{N} + k_0^2 \mathbf{N}}{j\omega\mu_0} \right\} \end{aligned}$$

²used to describe the macroscopic properties of the medium of interest

Cavity layout

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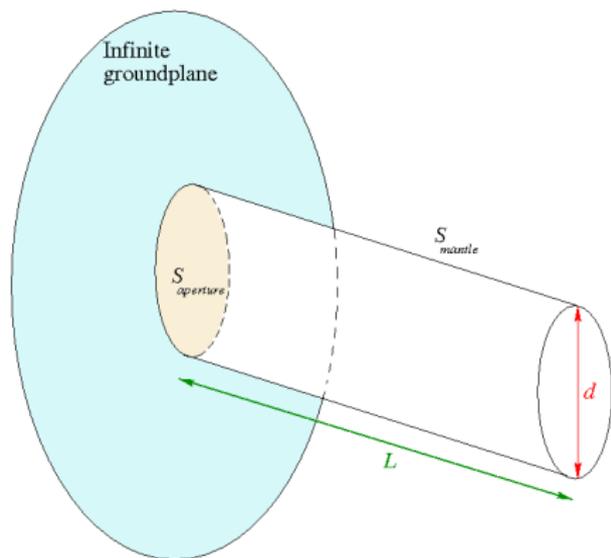
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Figure: Jet engine air intake is abstracted to a cylindrical one-side open ended cavity



$$(\hat{n} \times \mathbf{E})_{S_{\text{mantle}}} = 0$$

$$(\hat{n} \times \mathbf{H}^{\text{inc}})_{S_{\text{aperture}}} = 4\hat{n} \times \left\{ \frac{\nabla^2 \cdot \mathbf{N} + k_0^2 \mathbf{N}}{j\omega\mu_0} \right\}$$

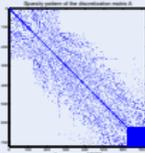
FEM discretization

Equation (1) is discretized by a higher order edge based finite element discretization method, resulting in a large linear system:

$$Au = f$$

Properties linear system:

- A consists of a sparse part and a fully populated part
- A is ‘nearly’ symmetric but not Hermitian
- A is ill-conditioned
- A is ‘highly’ indefinite



Present implementation

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- Dimension of system matrix $A : N \approx 1 \cdot 10^7$ (total number of unknowns)
- Iterative Krylov subspace method: *Generalized Conjugate Residual* (GCR) method
- Ill-conditioned matrix \Rightarrow improve convergence GCR by *shifted Laplace preconditioner*
- GCR long recurrence method \Rightarrow difficult to satisfy memory requirements for storing eigenvectors of Krylov basis

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Proposed solution:

Modify existing algorithm by using a *multigrid solution method* for the preconditioner system

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General

- Iterative solvers used in a lot of applications where large (non)linear systems arise from discretization of PDEs
- Suitable for parallel computing
- When system matrix ill-conditioned, no efficient direct application
- Rate of convergence independent of mesh size h
- Linear system of N unknowns can be solved in cN arithmetic operations (c constant)

Application of multigrid – Helmholtz equation

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Based on the work of Erlangga³:

- MG is a robust and efficient solver for the preconditioned Helmholtz equation in two and three dimensions
- Helmholtz and Maxwell's equation have similar properties
⇒ expected that MG will also be very effective in current application

³See my literature report for the complete reference

Analogy Helmholtz and vector wave equation

Homogeneous Helmholtz equation	Vector Helmholtz equation
$-\nabla^2 u - k_0^2 u = 0$	$-\nabla^2 \mathbf{E} - k_0^2 \mathbf{E} = 0$
Shifted Laplace preconditioner	Analogy of shifted Laplace preconditioner
$\mathcal{M}_{\beta_1, \beta_2} = -\nabla^2 u - \hat{k}^2 u = 0$	$\mathcal{W}_{\beta_1, \beta_2} = -\nabla^2 \mathbf{E} - \hat{k}^2 \mathbf{E} = 0$

$$\text{Recall: } \nabla \times \nabla \times \mathbf{E} - k_0^2 \mathbf{E} = -jk_0 Z_0 \mathbf{J}$$

(the vector Helmholtz equation is obtained using the vector identity)

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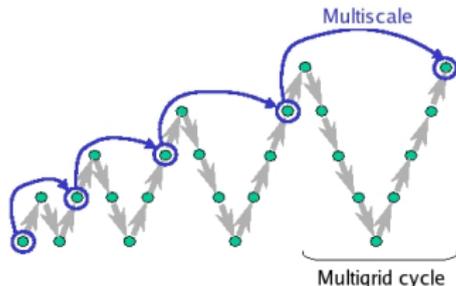
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Current application

- *Indirect* application of MG in current problem: used as solver for preconditioner system
- Unstructured grid \Rightarrow *algebraic multigrid*
- Using **AMG solver** \Rightarrow constant preconditioner \Rightarrow enables short recurrence method (e.g. BiCG-STAB)
- Short recurrence method \Rightarrow considerable storage reduction



Limited time

No time available to develop a dedicated AMG solver

AMG solvers available

As there are several AMG black box solvers available, the task is to choose the one most suitable for the current application

⇒ formulate requirements for black box solver

Requirements for black box AMG solver

For minimal effort to incorporate in the existing solution algorithm, the AMG black box should:

- be parallelizable
- be suitable for the vector processor of the NEC SX-8R machine
- have a matrix free implementation: in the existing implementation the element matrices are not assembled into the system matrix
- use the element matrices as input-parameter: they are available in the FEM approach and contain useful information

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Second part of the thesis

- choose suitable AMG black box solver
- incorporate AMG black box solver
- replace GCR by short recurrence method (e.g. BiCG-STAB)

