

# Efficient Computation of Flow with Cavitation with Compressible Pressure Correction

Objective: Efficient computation of flow with cavitation with simple engineering model

## Hydrodynamic Cavitation

Cavitation is the formation of vapor filled bubbles when due to the dynamics of the flow the local pressure in a liquid falls below the vapor pressure. Unsteady cavitation on lifting surfaces gives rise to:

- loss of performance
- noise
- vibrations
- erosion

## Model

We use the Homogeneous Equilibrium Model for two-phase liquid/vapor flow. In the HEM the following assumptions are made:

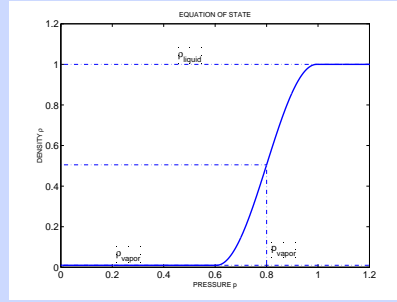
- Both phases are in thermodynamic equilibrium.
- Both phases are at saturation.
- The velocity slip between both phases is negligible.

## Governing equations

The HEM for inviscid isothermal flow is described by the following mass and momentum conservation equation and a barotropic equation of state for the water/vapor mixture:

$$\begin{aligned} \frac{\partial \rho}{\partial t} + (\rho u_\alpha)_{,\alpha} &= 0, \\ \frac{\partial \rho u_\alpha}{\partial t} + (\rho u_\alpha u_\beta)_{,\beta} &= -p_{,\alpha}, \\ \rho &= \rho(p). \end{aligned}$$

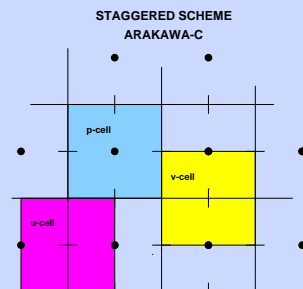
The system is unconditionally hyperbolic and the mixture equation of state is nonlinear and nonconvex:



The pure liquid and pure vapor phase are nearly incompressible, while the mixture phase is highly compressible. As a result the Mach number in the flow varies in the range  $0 \leq \text{Ma} \leq 30$ . This calls for a **Mach uniform method: A method that has accuracy and efficiency nearly uniform in the Mach number[1]**. A staggered discretisation in combination with a compressible pressure correction solution method has this desirable property.

## Discretisation

We use a finite volume discretisation, according to the staggered ARAKAWA-C arrangement:



## Compressible pressure correction

The pressure correction time-stepping method consists of the following stages: First the momentum equation is advanced in time, using the pressure at  $t^n$ .

$$\frac{m_\alpha^* - m_\alpha^n}{\delta t} + (u_\beta^n m_\alpha^*)_{,\beta} = -p_{,\alpha}^n,$$

The following pressure correction is postulated:

$$m_\alpha^{n+1} = m_\alpha^* - \delta t \delta p_{,\alpha}, \quad \delta p = (p^{n+1} - p^n),$$

and substituted in the mass conservation equation:

$$\frac{\rho(p^n + \delta p) - \rho^n}{\delta t} + (m_\alpha^* - \delta t \delta p_{,\alpha})_{,\alpha} = 0.$$

This nonlinear equation for the pressure correction is solved with a nonlinear Gauss-Seidel algorithm, accelerated by GMRES [2]. Finally pressure and momentum are updated:

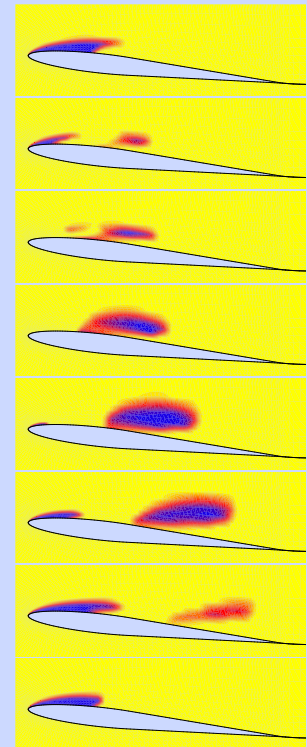
$$\begin{aligned} p^{n+1} &= p^n + \delta p, \\ m_\alpha^{n+1} &= m_\alpha^* - \delta t \delta p_{,\alpha}. \end{aligned}$$

## Results

Simulation of cavitation on EN-hydrofoil, cavitation number

$$\sigma = \frac{p_\infty - p_{\text{vapor}}}{\frac{1}{2} \rho_\infty U_\infty^2} = 1.2, \quad (1)$$

angle of attack  $\alpha = 6.2^\circ$ .



## References

- (1) H. Bijl & P. Wesseling J. Comp. Phys. 141:153-173 1998.
- (2) D.R. van der Heul, C. Vuik & P. Wesseling Comput Visual Sci 2:63-68 1999.



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