

Acceleration of Turbomachinery steady CFD Simulations on GPU

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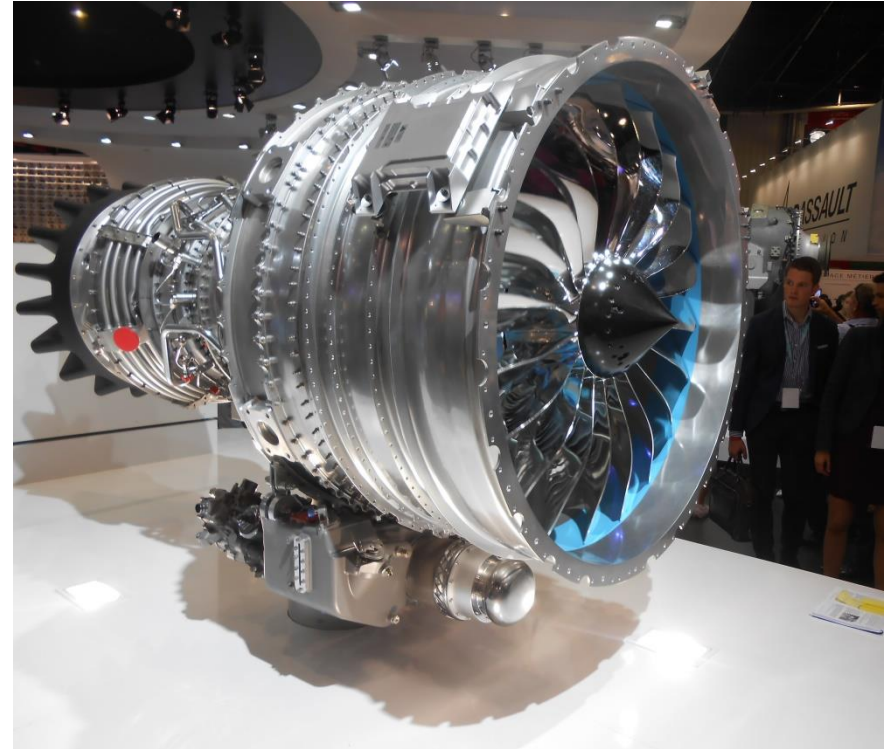
Unconventional HPC,
EuroPar 2016 WS
Grenoble, 23.08.2016

Topic of Interest:
Reduce Fuel Consumption and CO₂ Emission

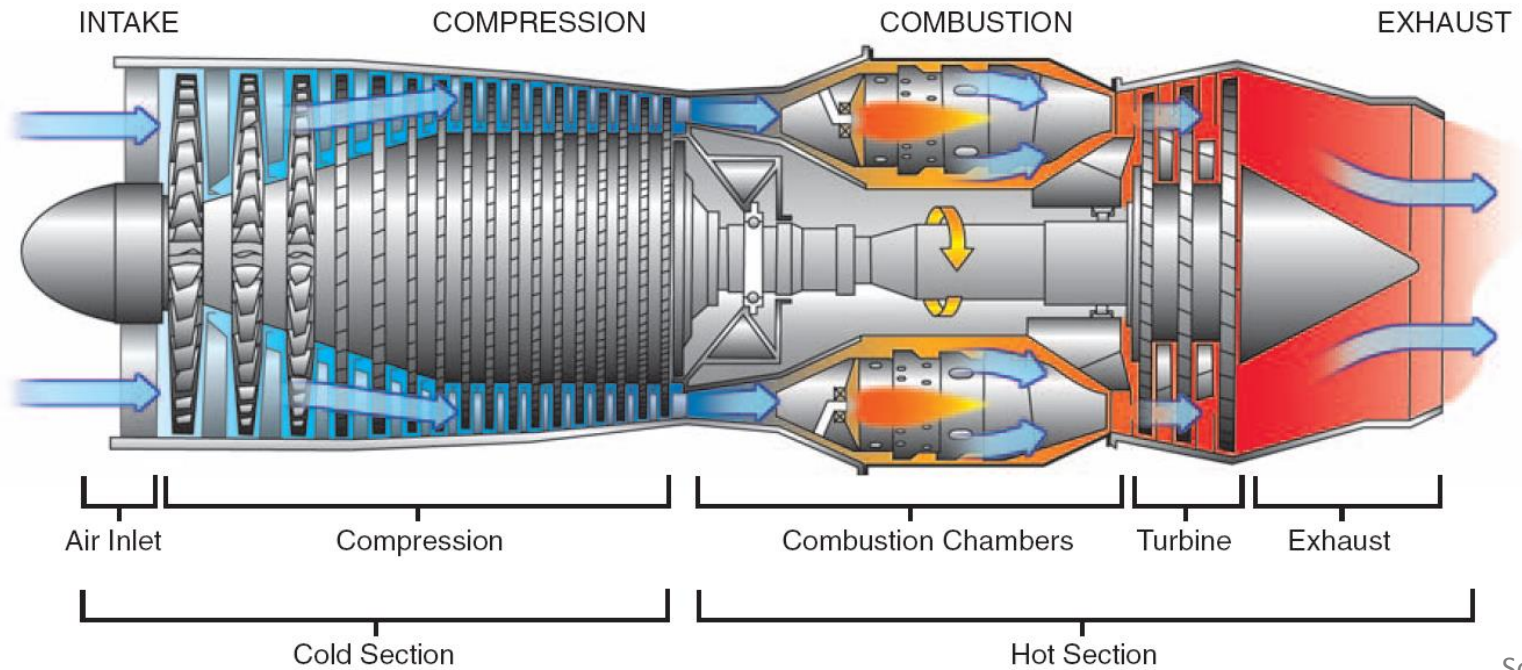


Wikipedia.org

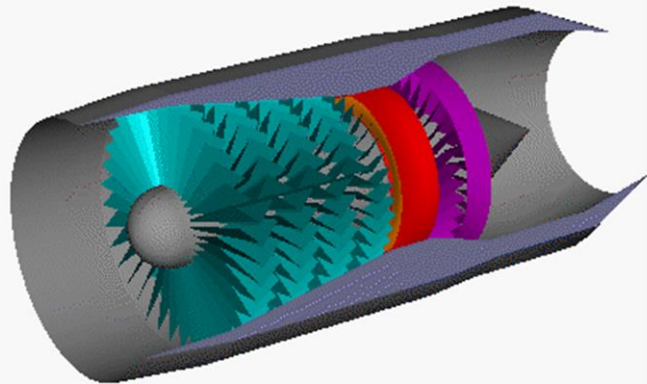
Turbomachinery is about Performance and Efficiency



Axial Jet Engine



Source:
Wikipedia.org



Content

- Multidisciplinary Optimization
- CFD simulations on GPU
 - Literature review
 - Implicit RANS Implementation
 - Benchmark
- Optimization Case

Optimization algorithm

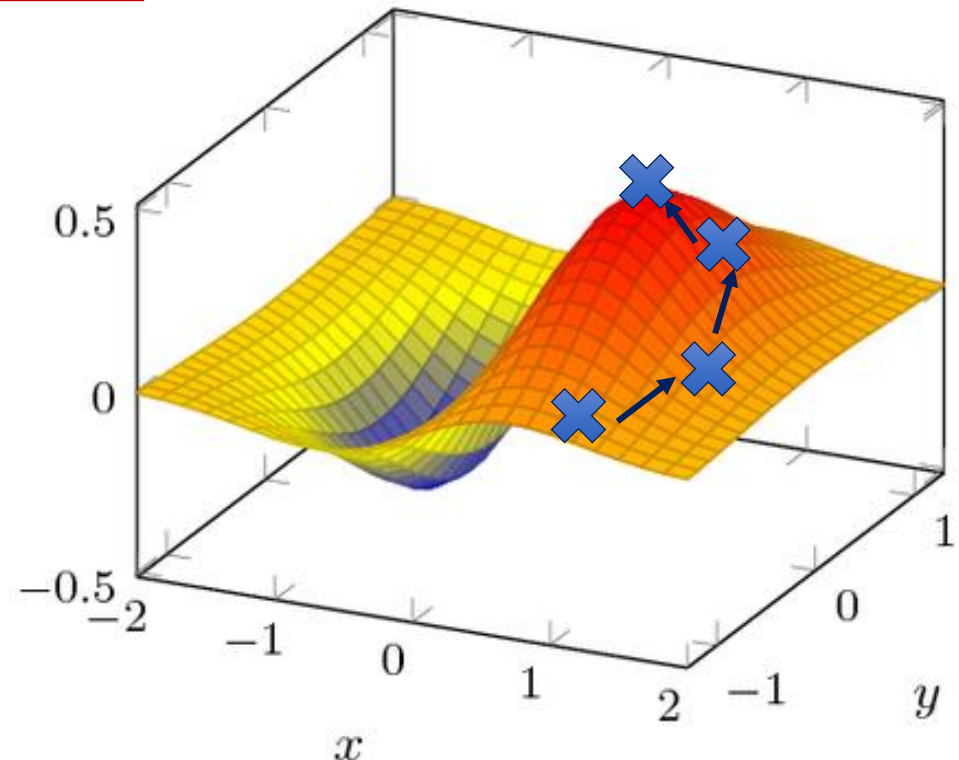
Derivative-based optimization

- fast convergence but ..
- derivative evaluation could be complicated and problem specific (adjoint, automatic differentiation)

Derivative free methods: e.g. Population based

- Simplicity
- Black box approach of the evaluation but ..
- Large number of evaluations

$\min f(\mathbf{x})$
subject to
 $g(\mathbf{x}) \leq 0$



Optimization algorithm

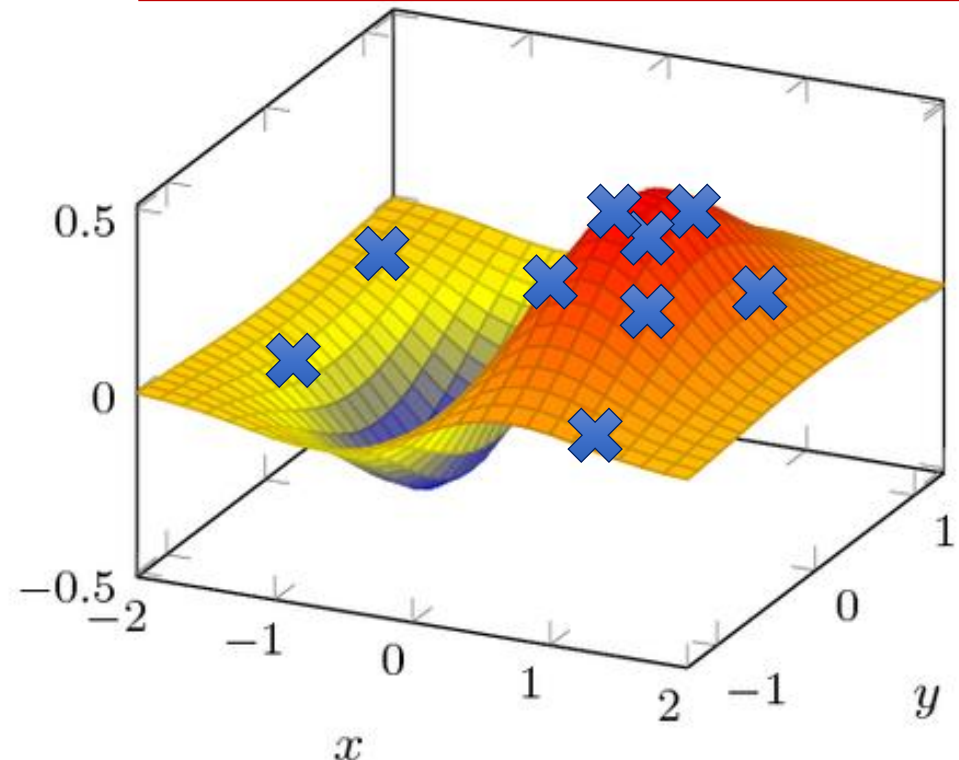
Derivative-based optimization

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Derivative free methods: e.g. Population based

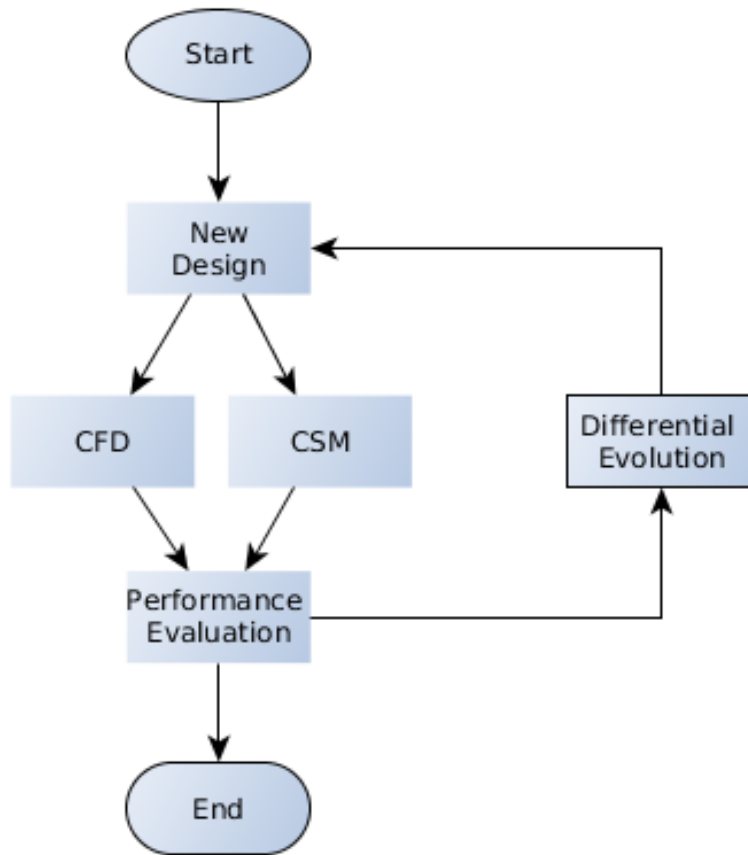
- Simplicity
- Black box approach of the evaluation but ..
- Large number of evaluations

$$\begin{aligned} &\min f(\mathbf{x}) \\ &\text{subject to} \\ &g(\mathbf{x}) \leq 0 \end{aligned}$$

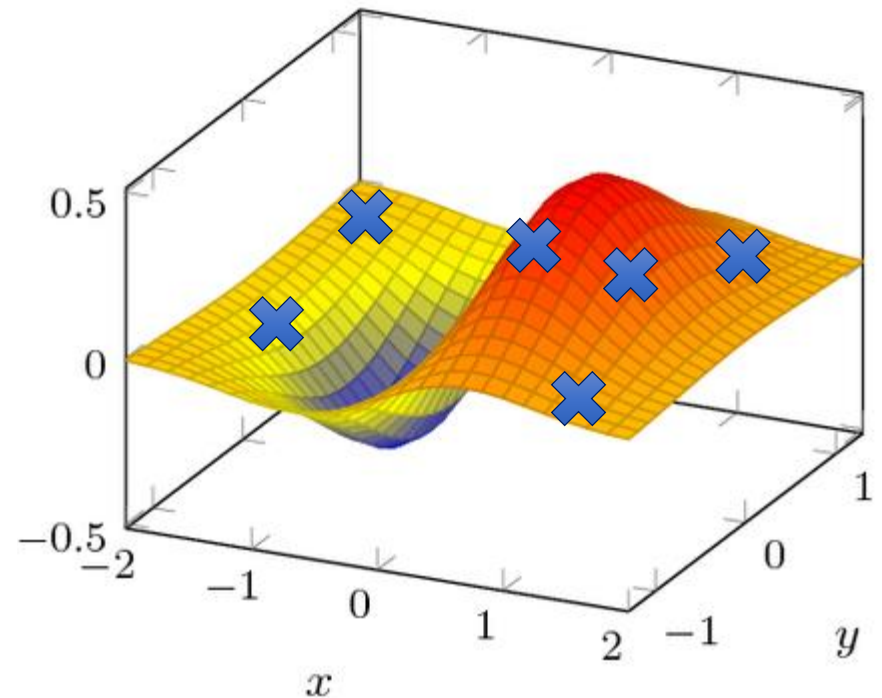


CFD: Core of the Optimization

CFD much slower than CSM
Need for acceleration -> GPU

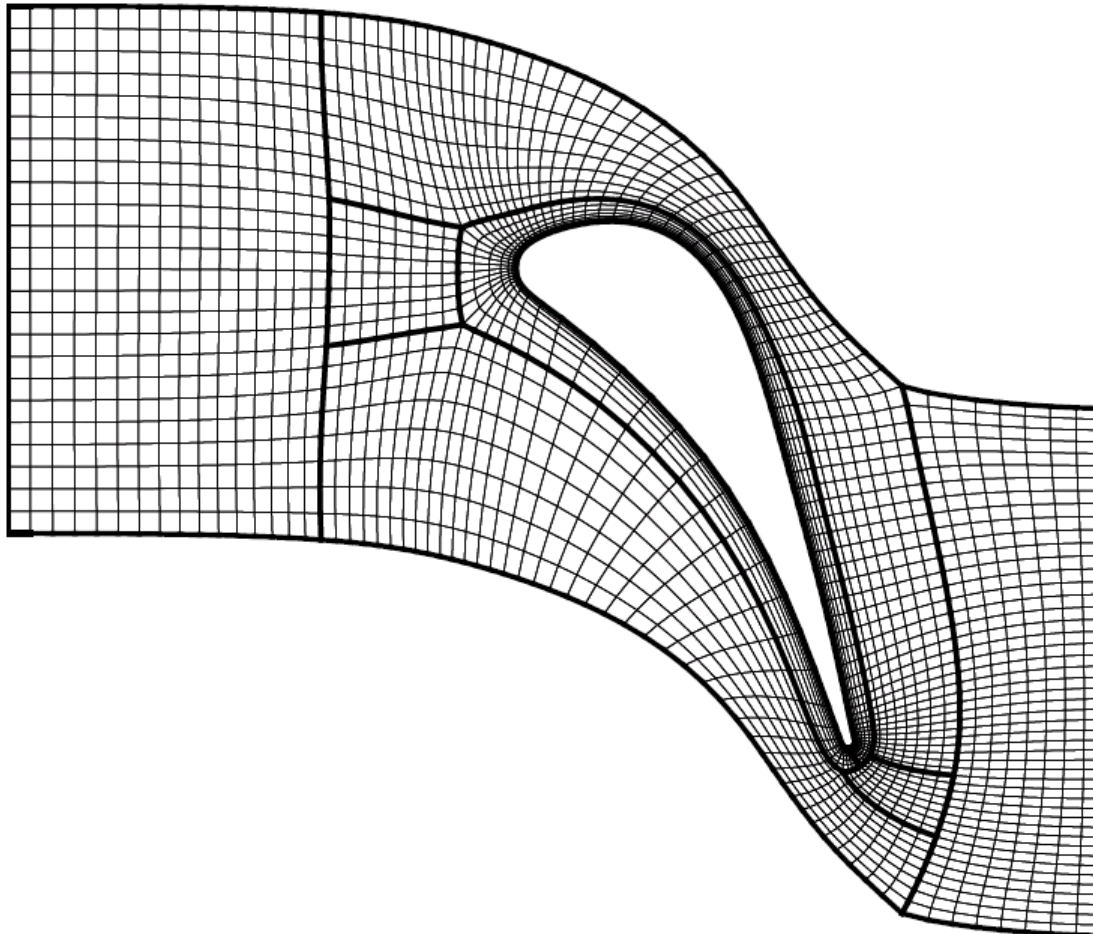


CADO: the VKI in-house optimizer



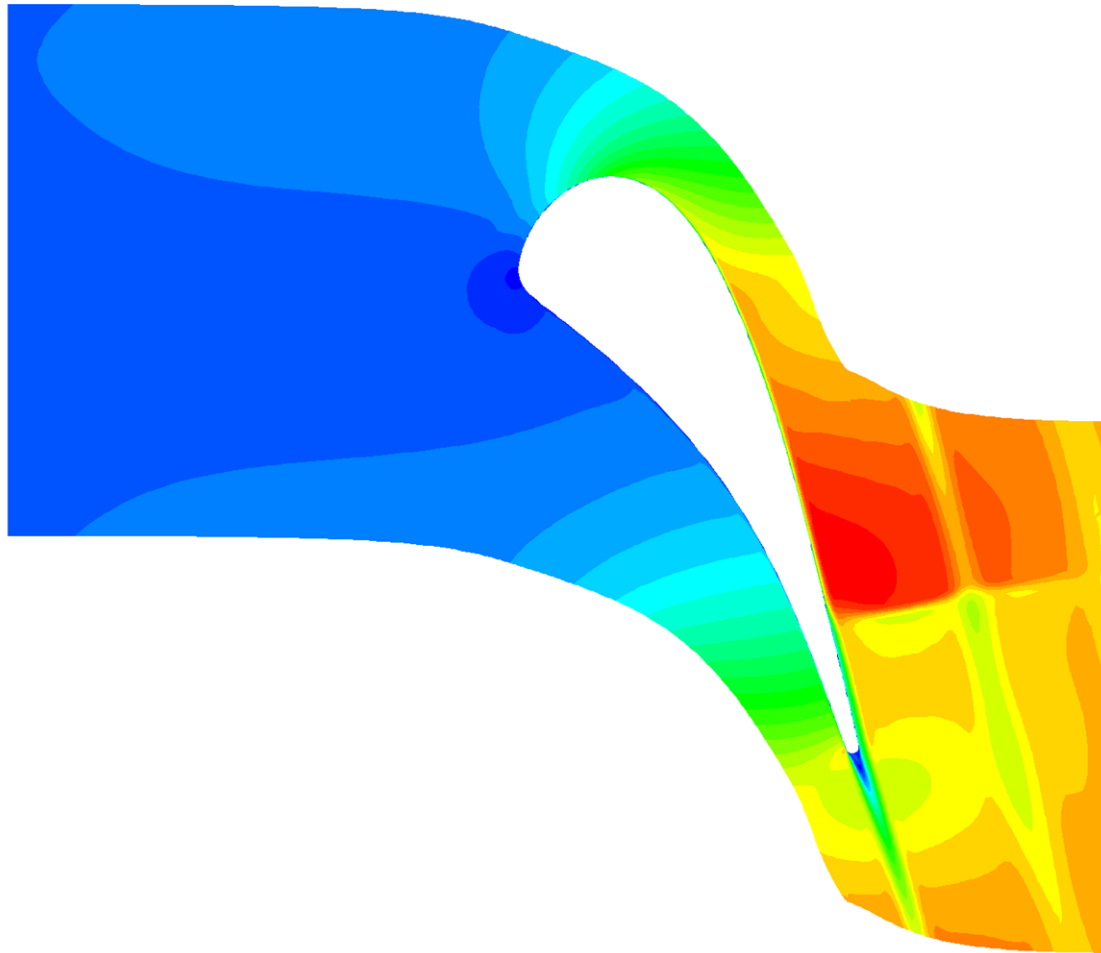
Steady CFD Simulations

- Simulation with a unique solution for given boundary Conditions.
- A start solution is advanced iteratively in time until convergence



Steady CFD Simulations

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- A start solution is advanced iteratively in time until convergence



Numerical Scheme:

$$\frac{\partial}{\partial t} \int_{\Omega} \mathbf{W} d\Omega + \oint_{\partial\Omega} (\mathbf{F}_c - \mathbf{F}_v) dS = \int_{\Omega} Q d\Omega \quad \mathbf{W} = \{\rho, \rho V_x, \rho V_y, \rho V_z, \rho E\}$$

$$\frac{(\Omega \bar{M})_I}{\Delta t_I} \Delta \vec{W}_I^n = -\beta \vec{R}_I^{(n+1)} - (1 - \beta) \vec{R}_I^n$$

Explicit Time Stepping ($\beta=0$):

$$\Delta \mathbf{W}^n = -\frac{\Delta t}{\Omega} \mathbf{R}^n$$

Implicit Time Stepping ($\beta=1$):

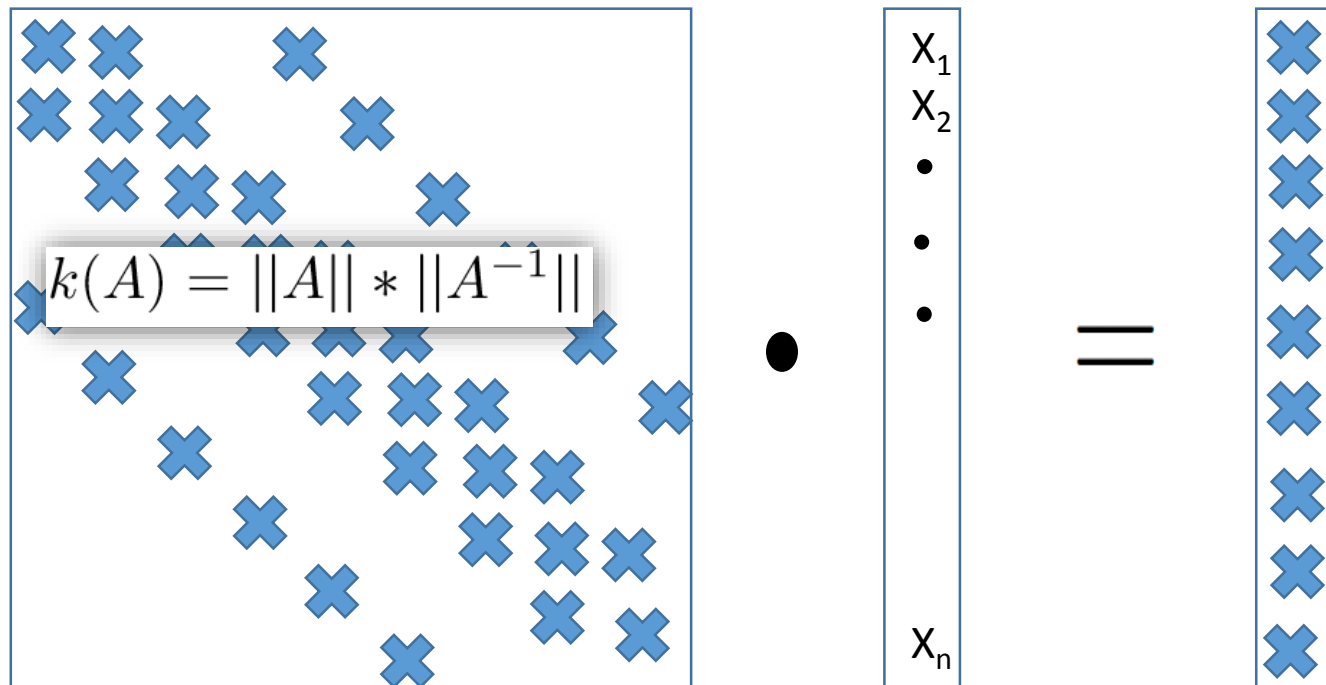
$$\vec{R}_I^{n+1} \approx \vec{R}_I^n + \left(\frac{\delta \vec{R}}{\delta \vec{W}} \right)_I \Delta \vec{W}^n$$

$$\left[\frac{(\Omega I)}{\Delta t} + \left(\frac{\delta \mathbf{R}}{\delta \mathbf{W}} \right) \right] \Delta \mathbf{W}^n = -\mathbf{R}^n$$

Implicit Time Stepping is more Stable but ...

$$\left[\frac{(\Omega I)}{\Delta t} + \left(\frac{\delta R}{\delta W} \right) \right] \Delta W^n = -R^n$$

$$A x = b$$



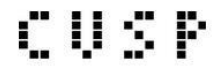
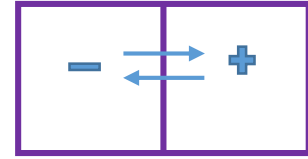
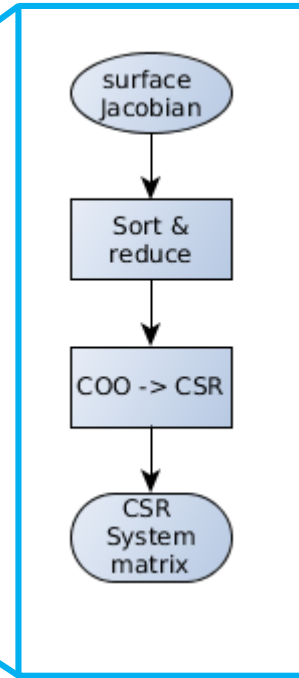
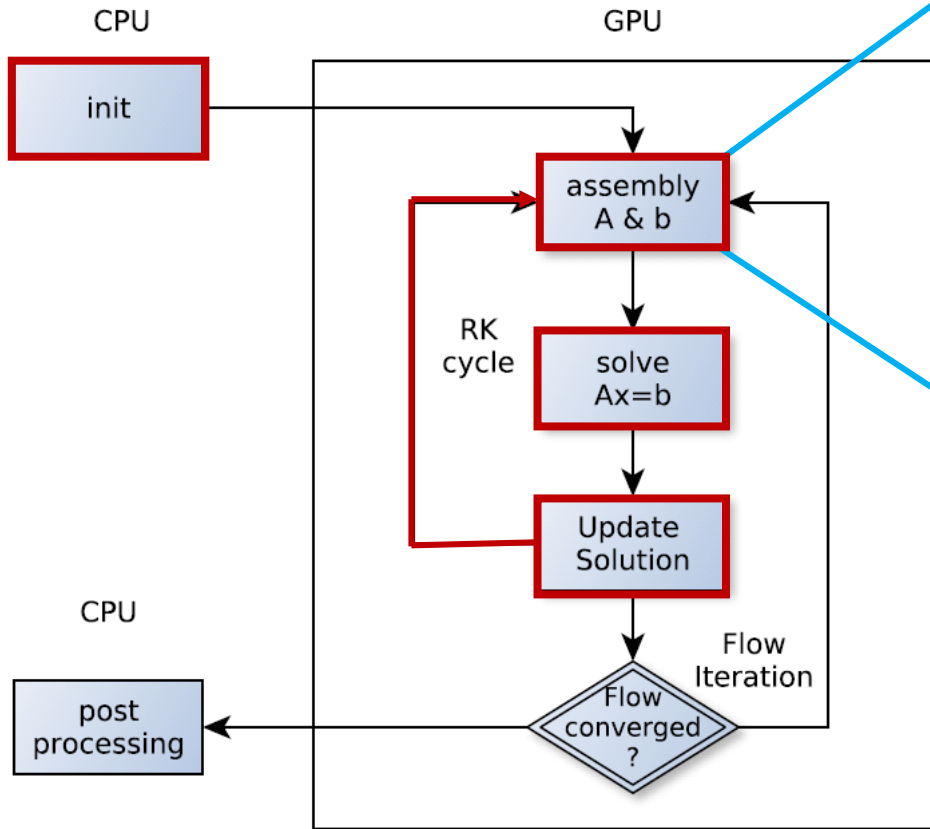
$$M^{-1} A x = M^{-1} b$$

Literature Review

- What to Port
 - only linear solver when it is dominant
 - both assembly and solve is optimal (no communication)
- Linear solver
 - Library : code maturity but restrictive
(petsc-dev, Paralution, AmgX, ViennaCL ...)
 - Own code: flexibility
- Storage format
 - Standard (CSR, DIA ...)
 - New (hybrid)

CFD Solver (Standard)

$$\left[\frac{(\Omega I)}{\Delta t} + \begin{pmatrix} \delta R \\ \delta W \end{pmatrix} \right] \Delta W^n = -R^n$$

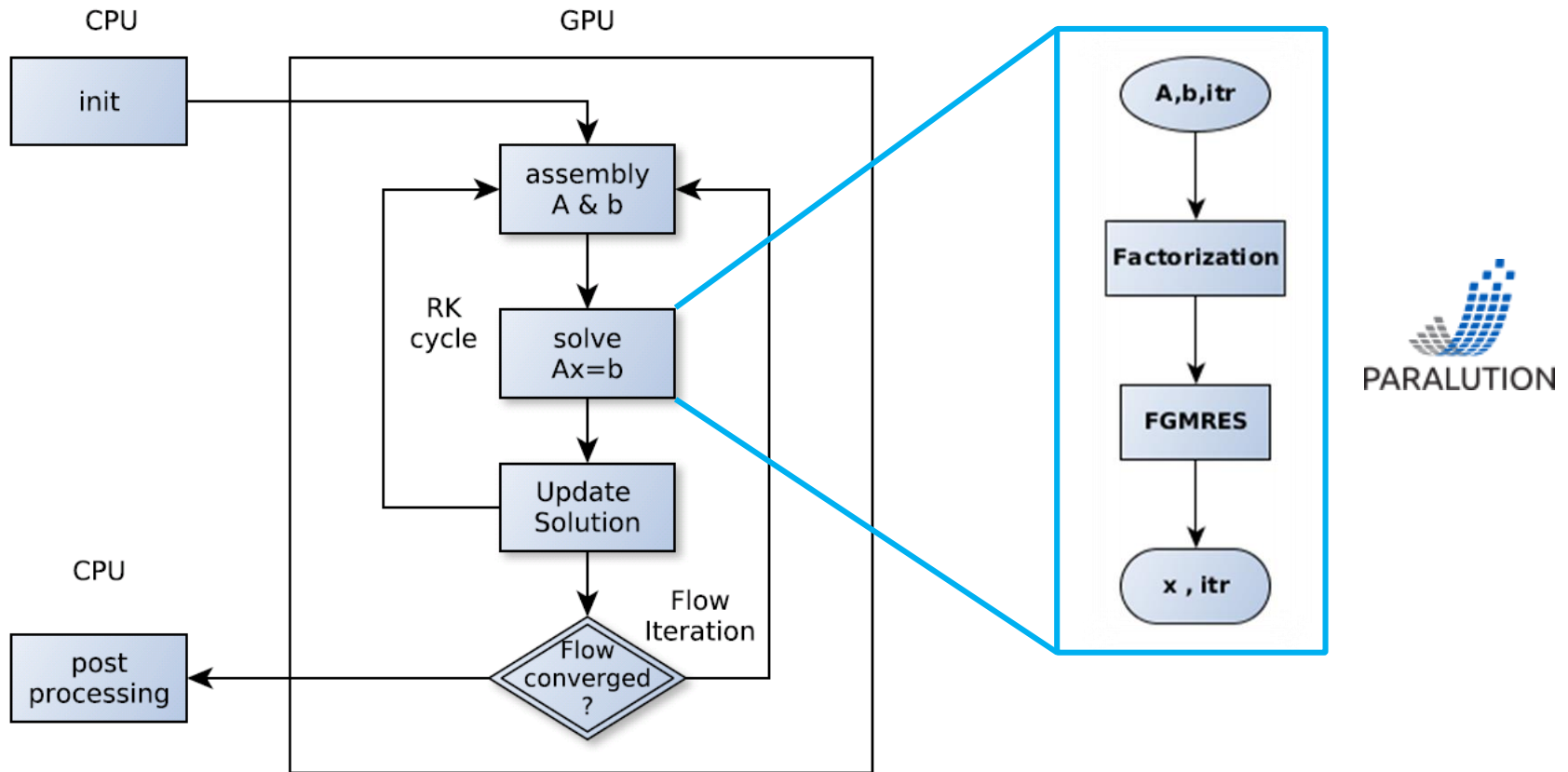


Implicit Runge-Kutta scheme

Xu et Al. JCP 2015

$$\begin{aligned}
 W^{(0)} &= W^n \\
 A^{(0)}[W^{(1)} - W^{(0)}] &= -\alpha_1 R(W^{(0)}) \\
 A^{(0)}[W^{(2)} - W^{(0)}] &= -\alpha_2 R(W^{(1)}) \\
 &\vdots \\
 A^{(0)}[W^{(m)} - W^{(0)}] &= -\alpha_m R(W^{(m-1)}) \\
 W^{n+1} &= W^{(0)} + [W^{(m)} - W^{(0)}]
 \end{aligned}$$

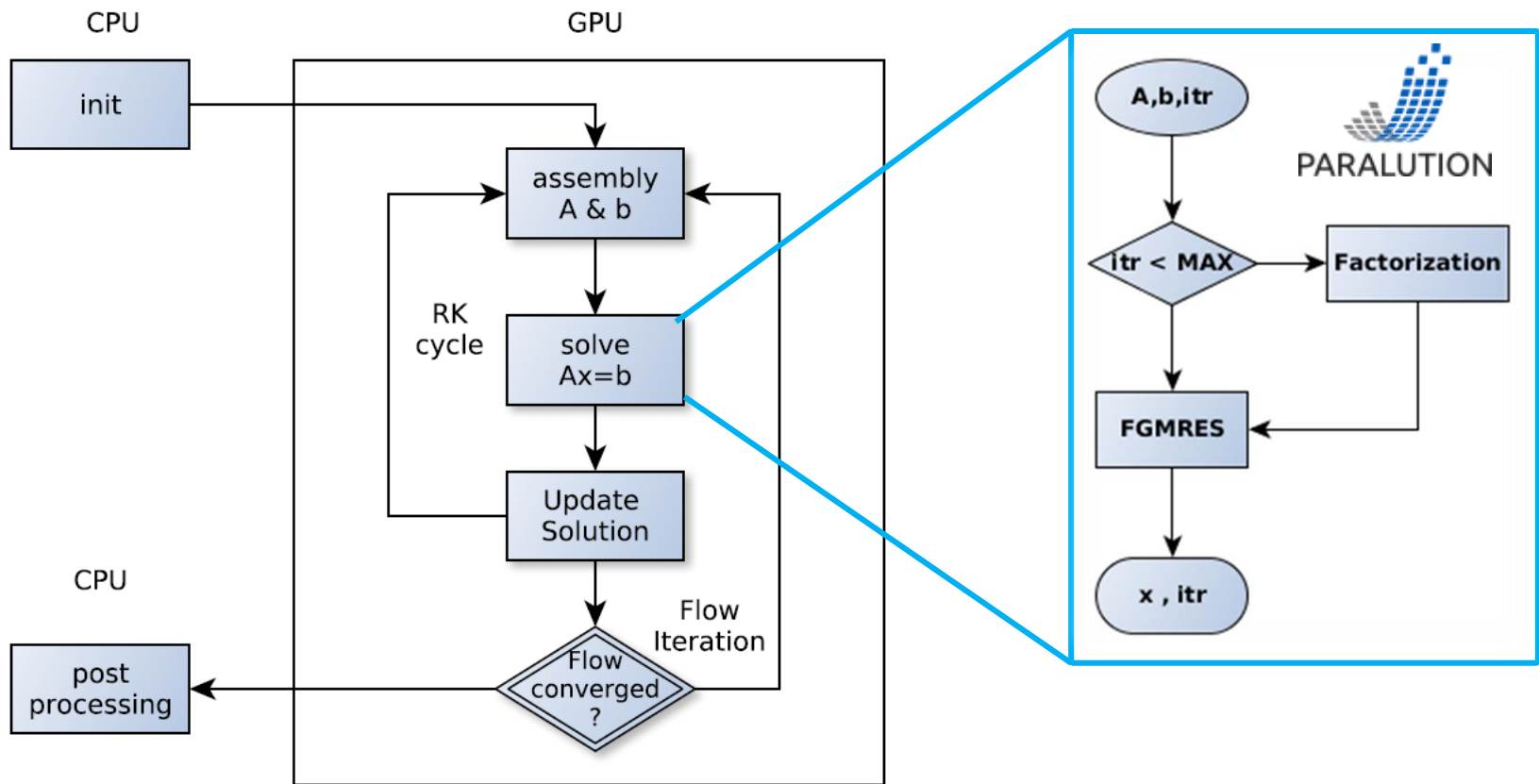
CFD Solver (Standard)



Implicit Runge-Kutta scheme

$$\begin{aligned}
 \mathbf{W}^{(0)} &= \mathbf{W}^n \\
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 \end{aligned}$$

CFD Solver (*On-demand* Factorization)



Implicit Runge-Kutta scheme

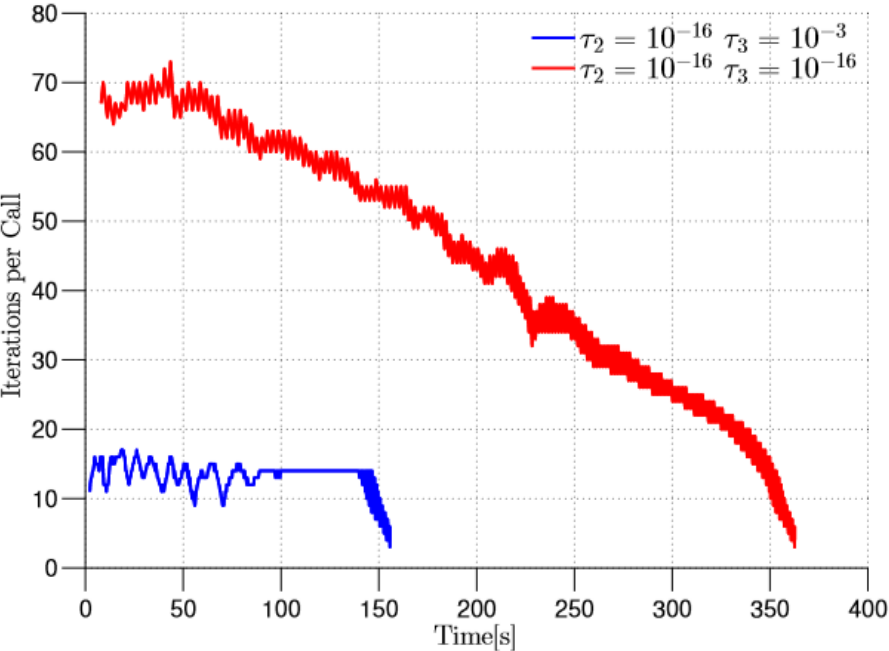
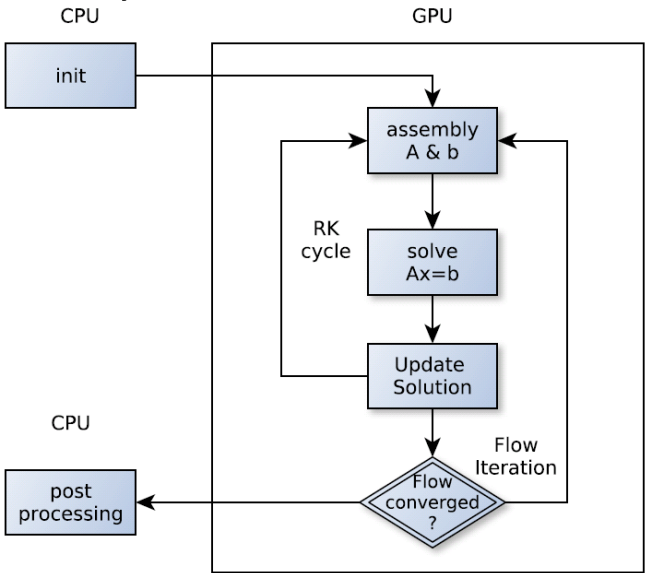
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 \end{aligned}$$

CFD Solver (*On-demand* Factorization)

$$r = Ax - b$$

Stop condition relative, absolute or a combination

$$\frac{\|r_k\|}{\|b\|} < \tau_3 \quad \|r_k\| < \tau_2$$

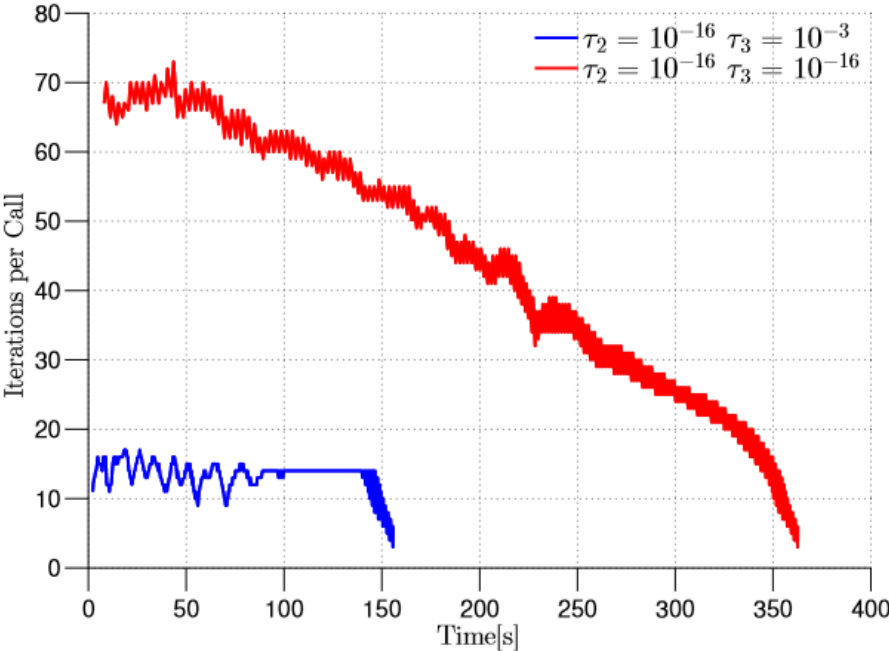
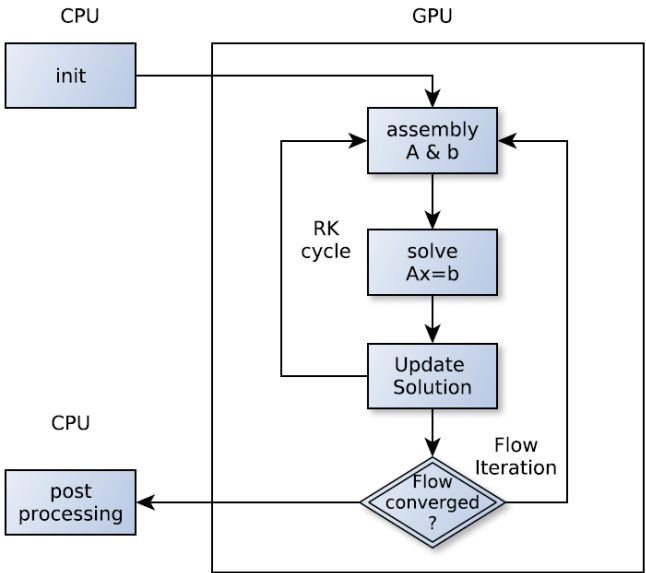


CFD Solver (*On-demand* Factorization)

$$r = Ax - b$$

Stop condition relative, absolute or a combination

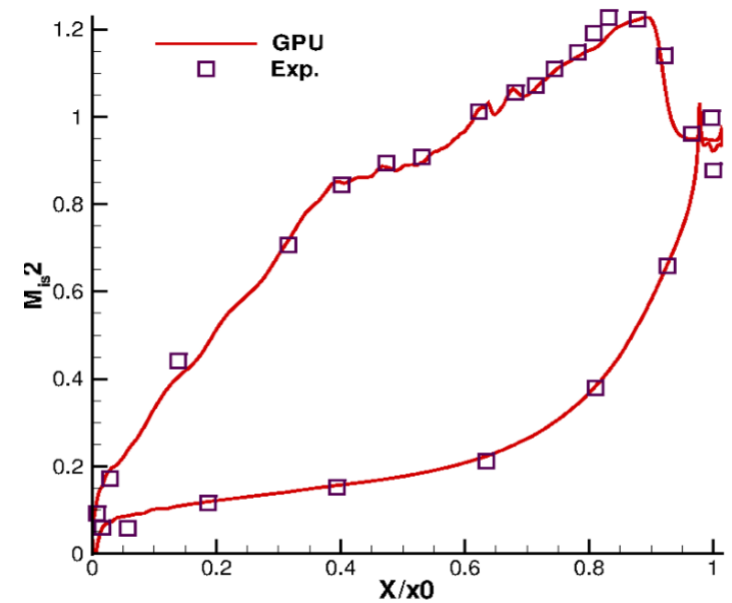
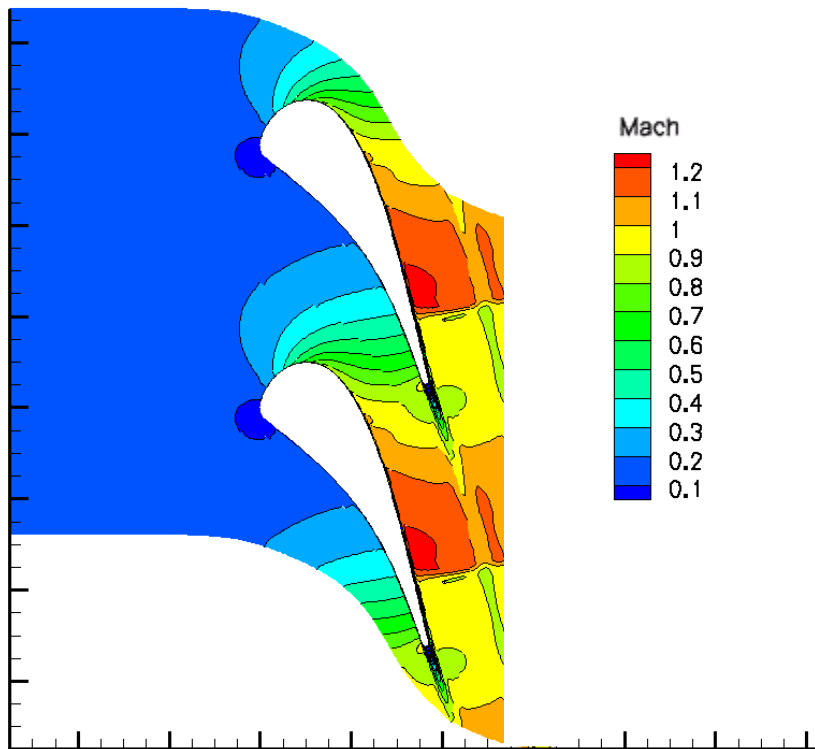
$$\frac{\|r_k\|}{\|b\|} < \tau_3 \quad \|r_k\| < \tau_2$$



$$MAX_ITR = \alpha * \frac{1}{m} \sum_{1}^m N_{ITR_i}$$

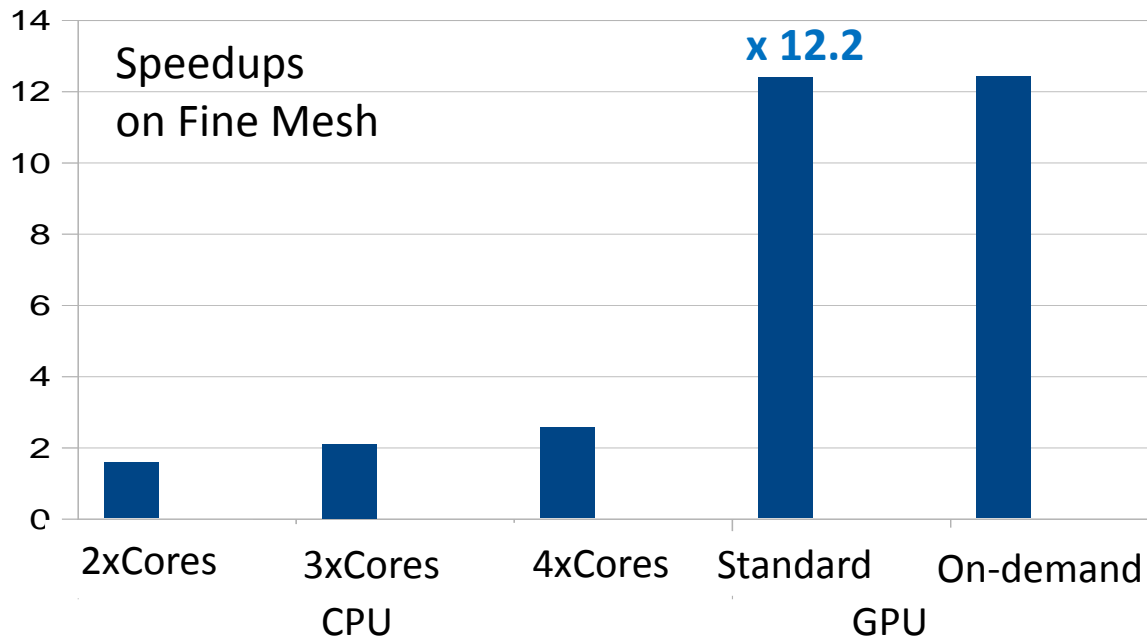
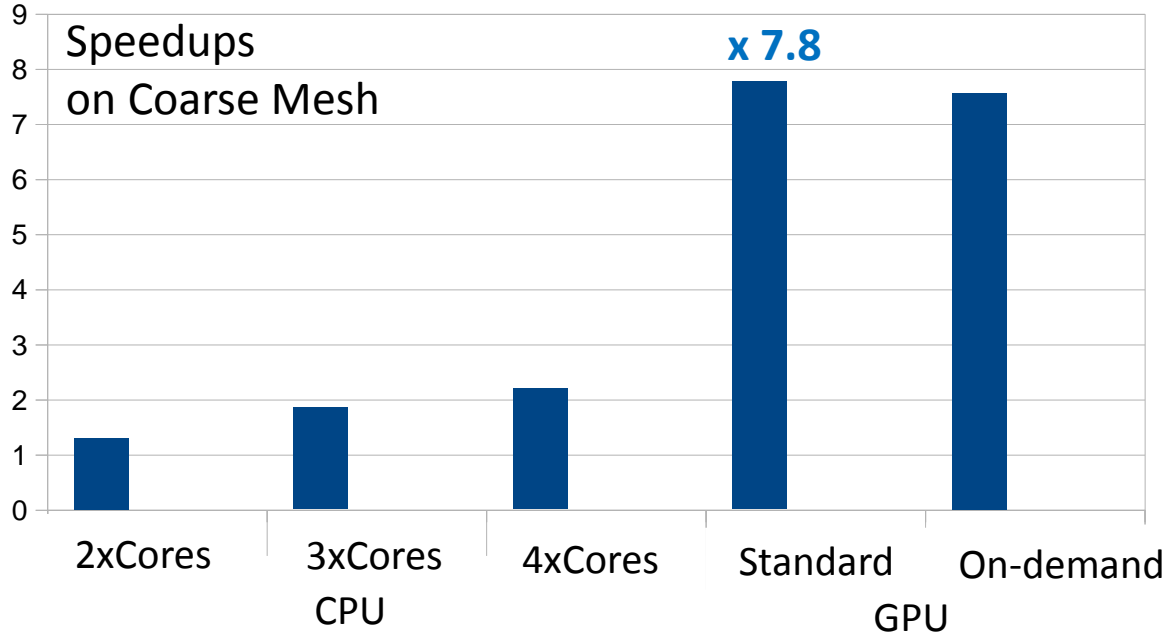
Benchmark: Flow around LS89

2-Stages Runge-Kutta

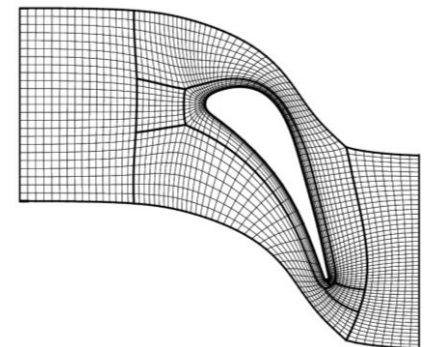
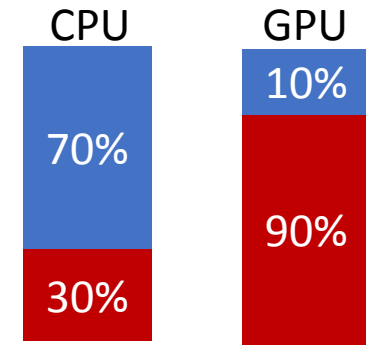


Mesh	N_{Cells}	N_{Rows}	nnz	nnz/row
Coarse	40k	200k	5.7M	[20 .. 30]
Fine	300k	1500k	52.6M	[20 .. 35]

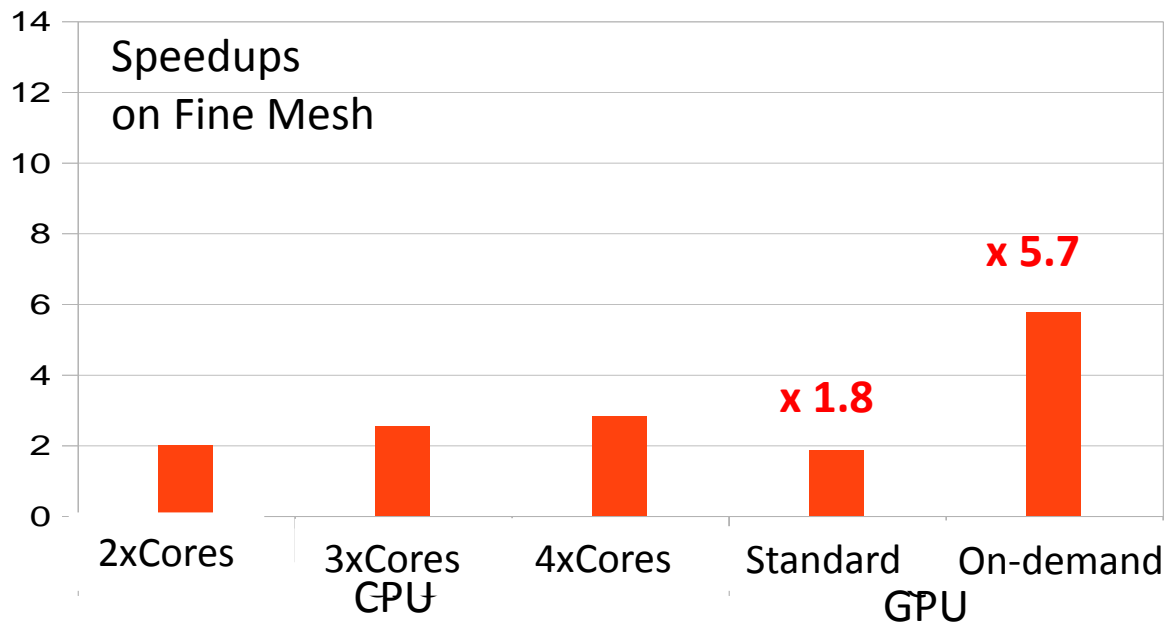
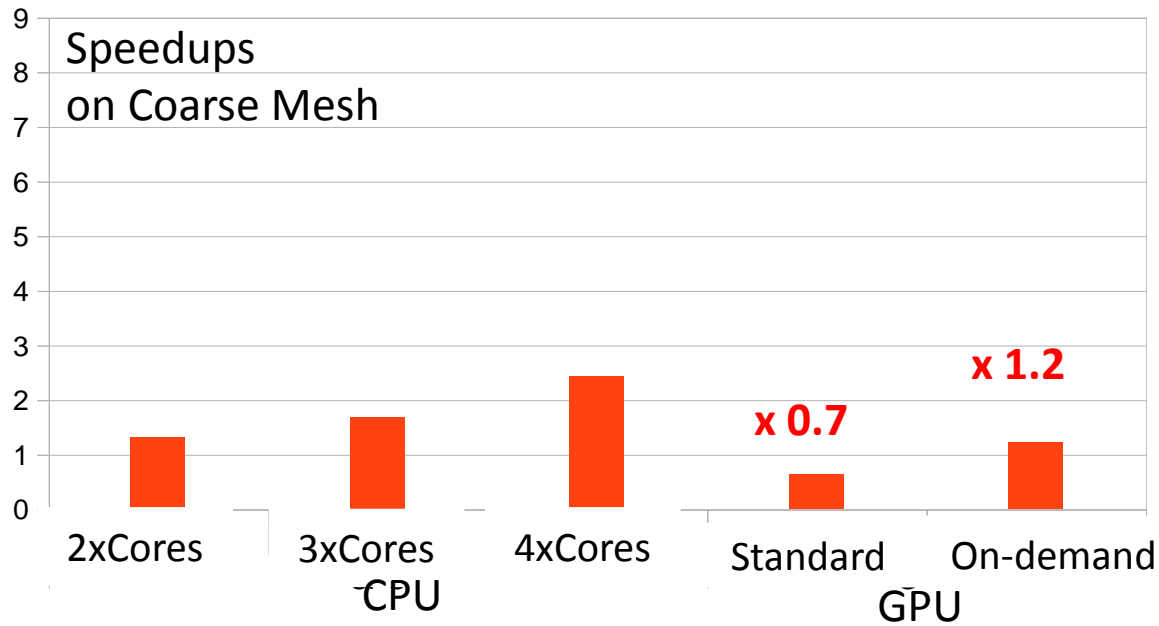
Assembly Acceleration



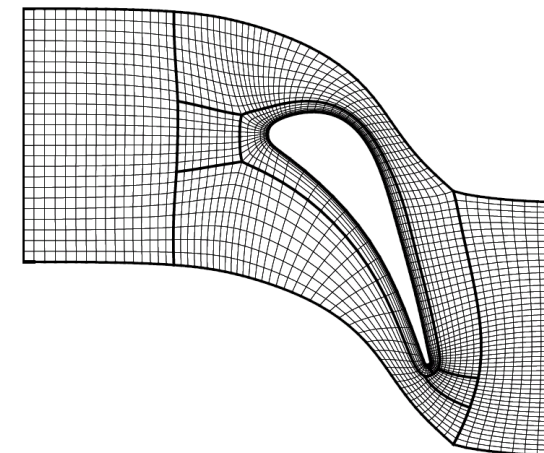
- Assembly speedup
- Linear solve speedup
- Global speedup



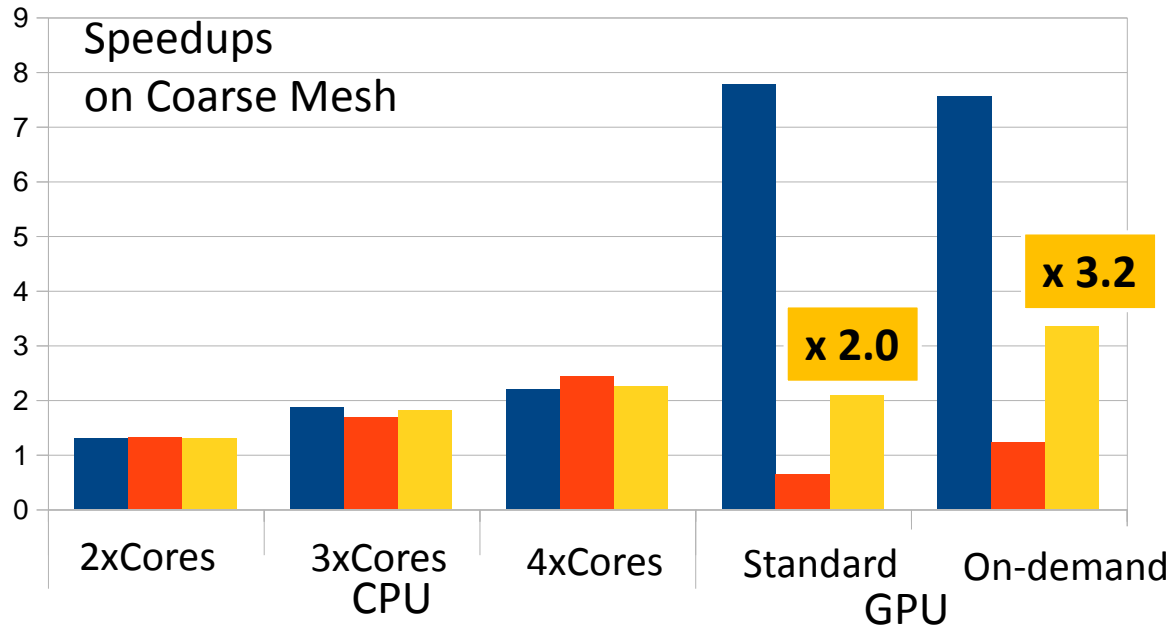
Linear Solver Acceleration



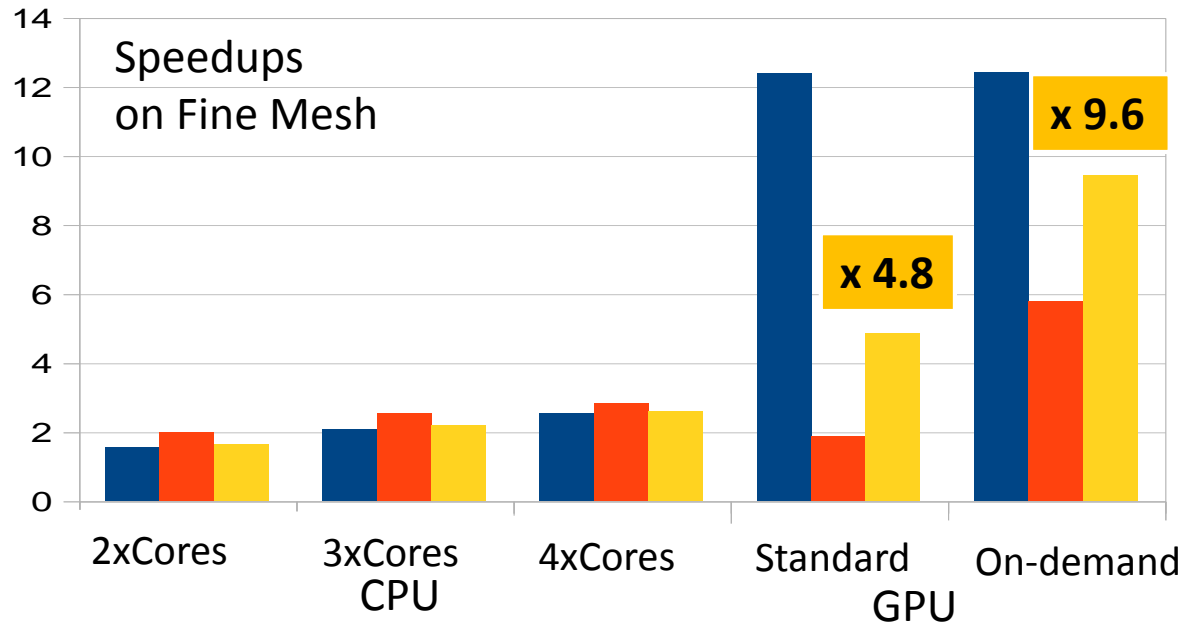
- Assembly speedup
- Linear solve speedup
- Global speedup



Global Acceleration

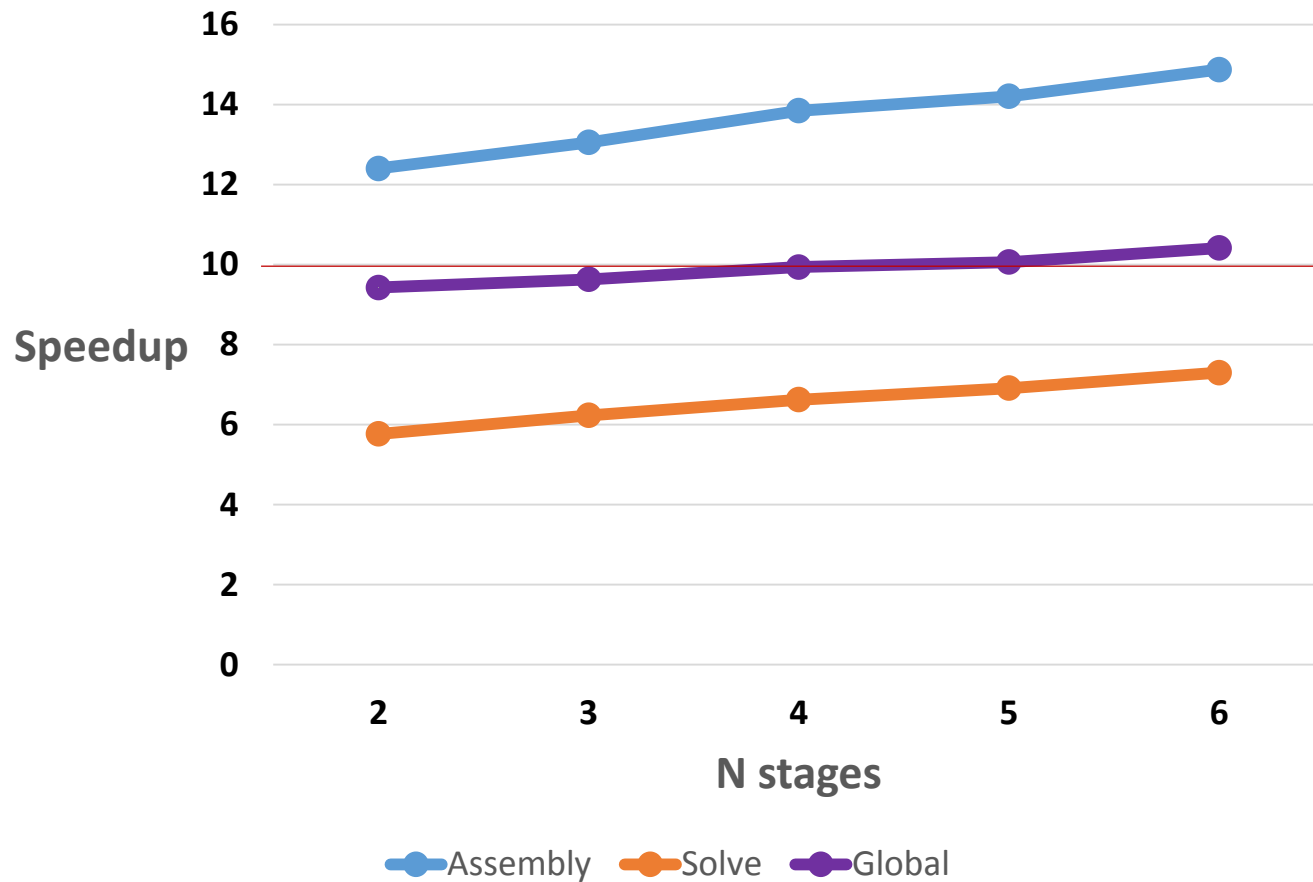


- Assembly speedup
- Linear solve speedup
- Global speedup



Suggestion for better Performance assessment are very welcome!

Increase of the Speedup for higher Numbers of Runge-Kutta Stages on Fine Mesh

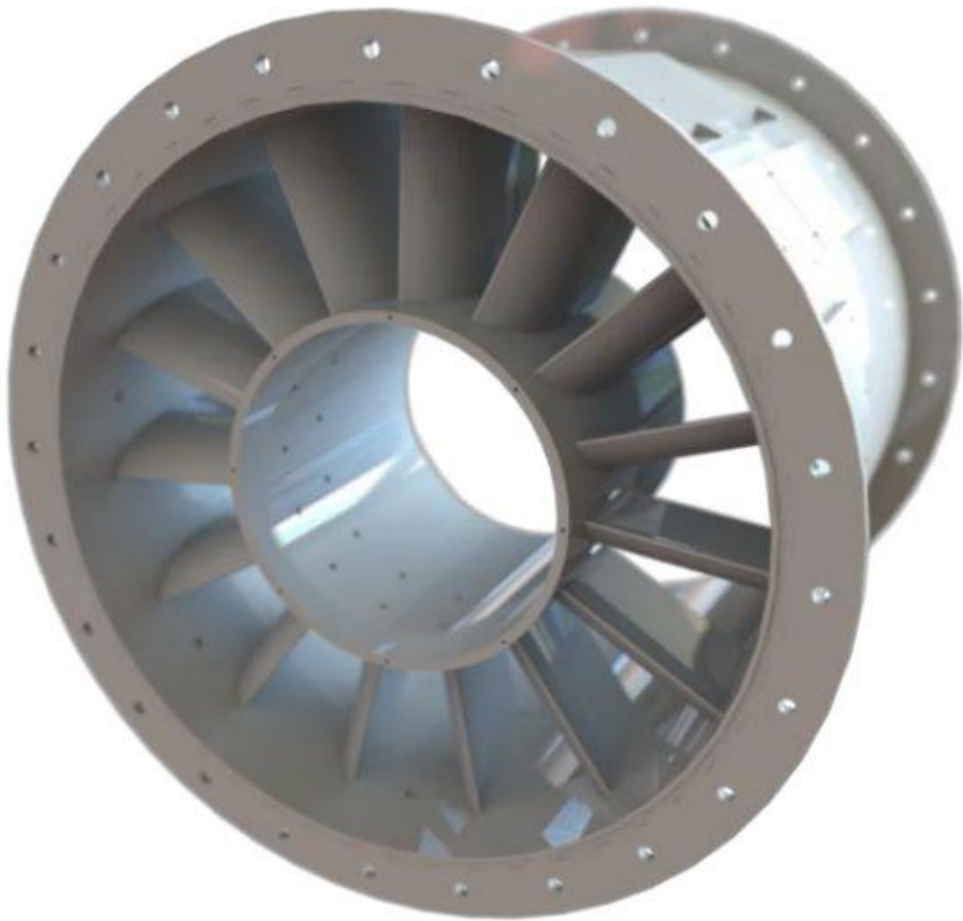


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 - Benchmark
- **Optimization Case**

Test Case 3: TU Berlin TurboLab Stator

Optimization requirements



Objectives:

- Decrease outflow axial deviation
- Decrease total pressure loss

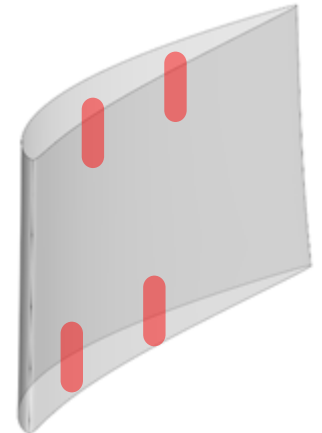
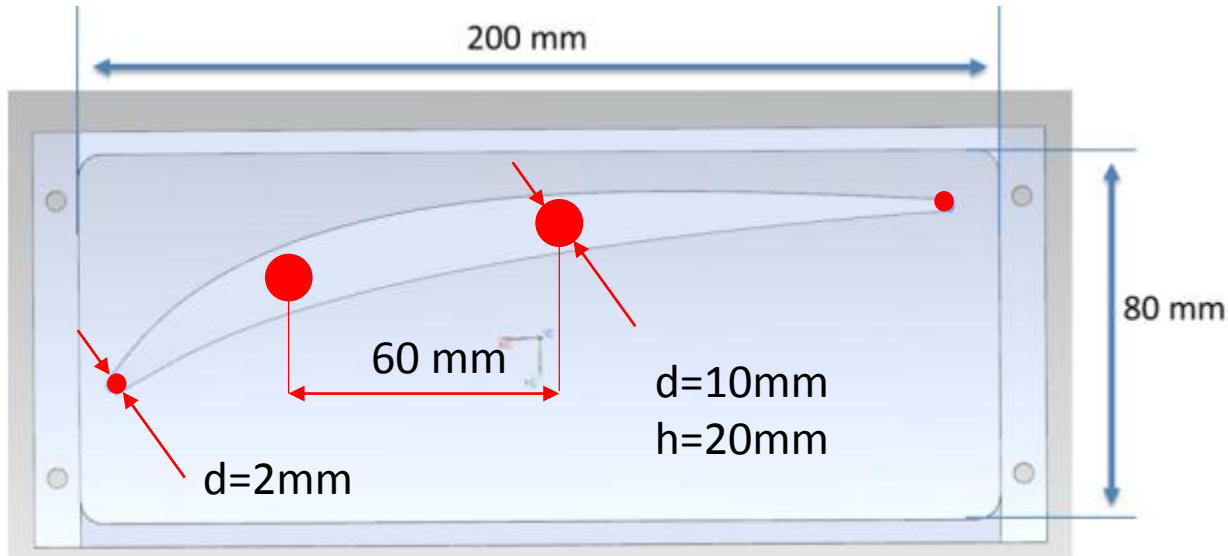
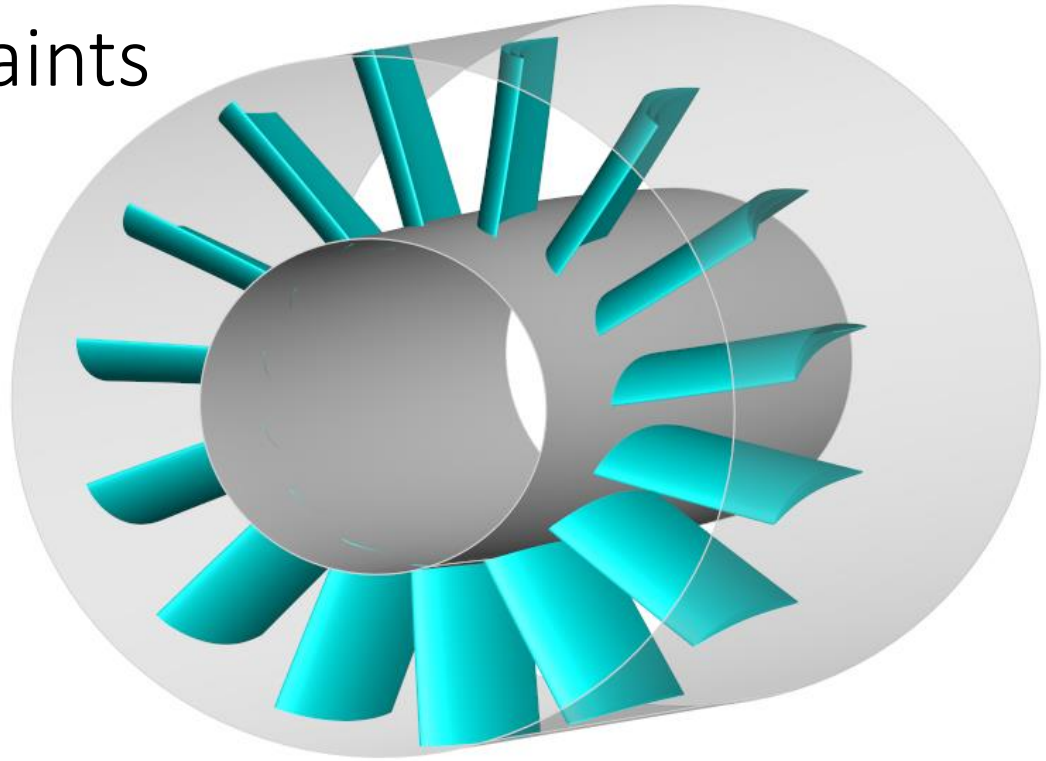
Considering 3 operating points

TurboLab

Manufacturing Constraints

- $N_{\text{blades}} = 15$
- Chord length fixed

- Casing fixture



TurboLab: Boundary conditions and summary

Inlet P_0 : 102713.0 Pa
Inlet T_0 : 294.314 K

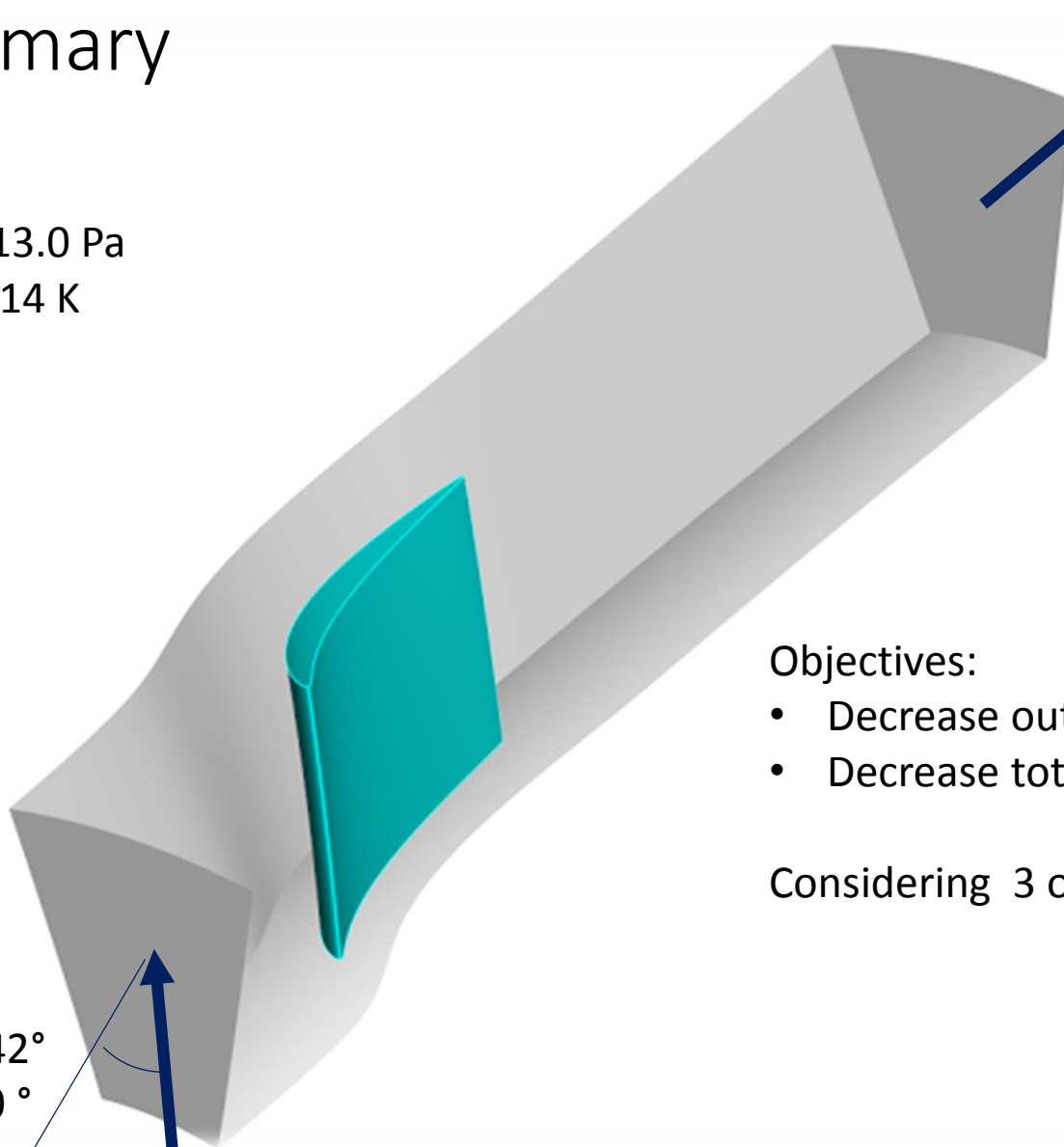
9 kg/s +/- 0.1
Massflow imposed
 P_2 adapted

Objectives:

- Decrease outflow axial deviation
- Decrease total pressure loss

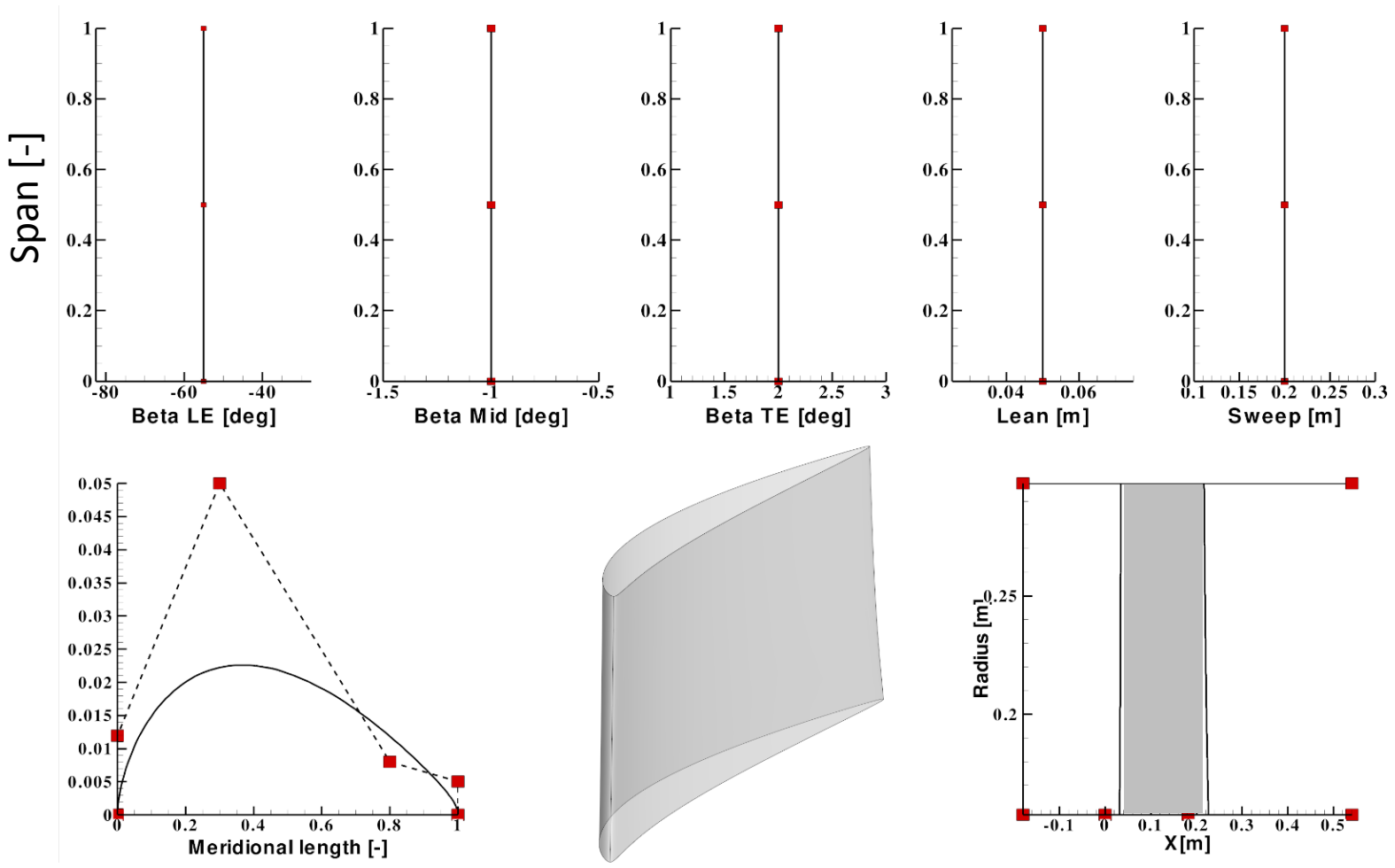
Considering 3 operating points

Inlet whirl angle: 42°
Inlet pitch angle: 0°

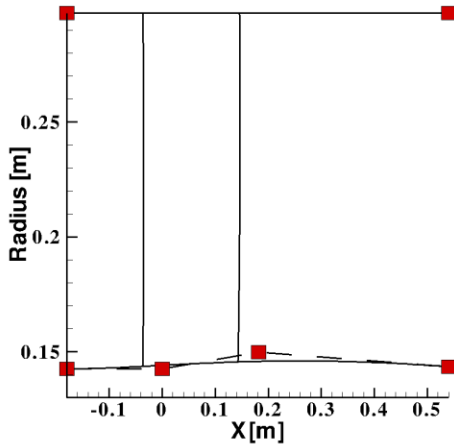
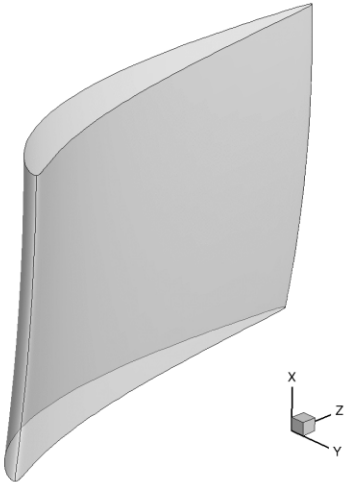
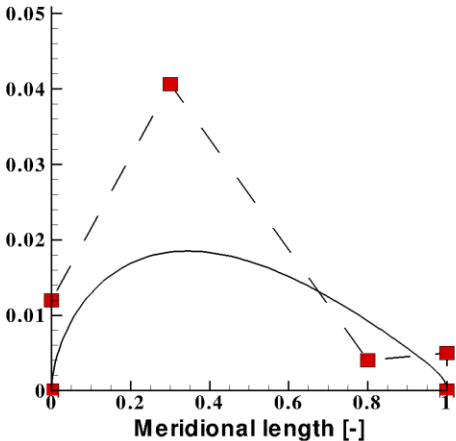
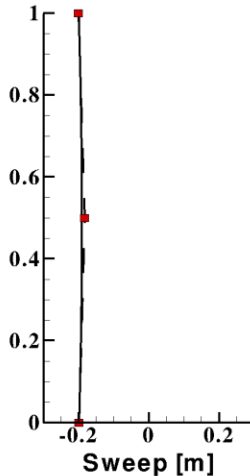
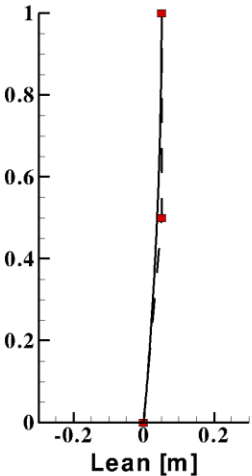
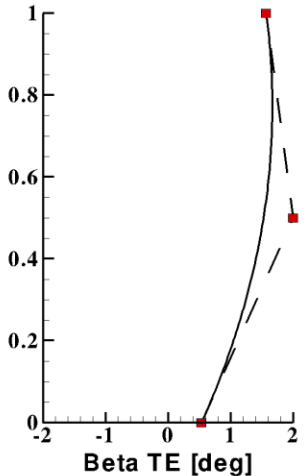
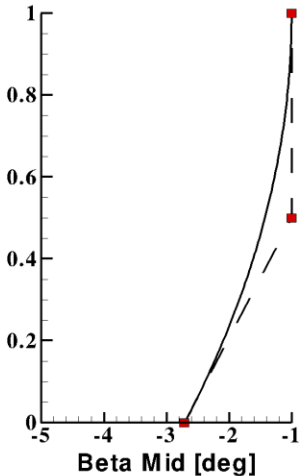
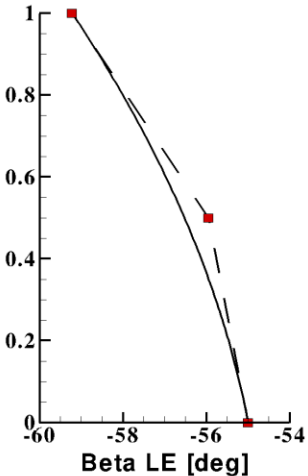


Parametrization

21 Design variables

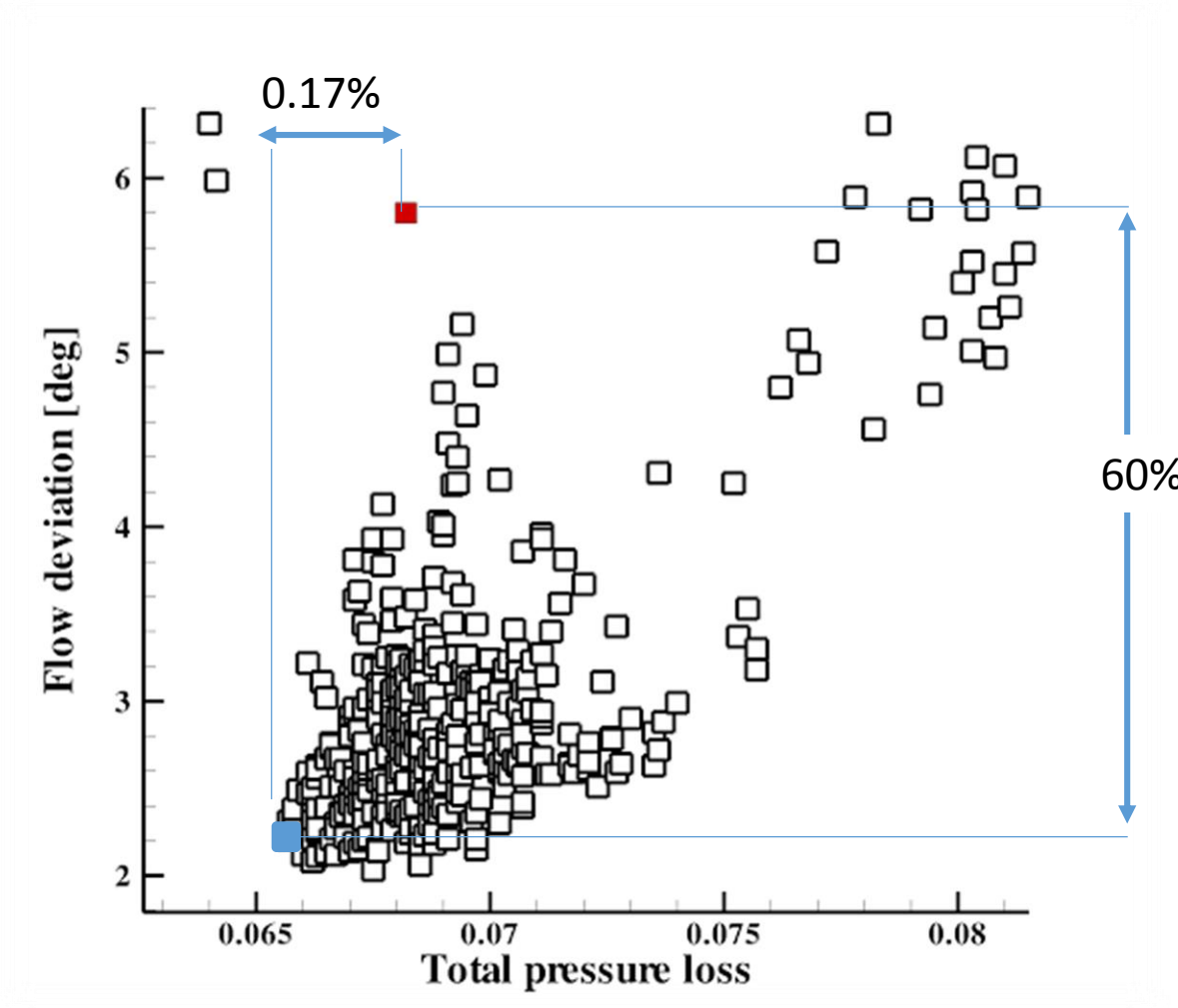


Turbolab Parameterization



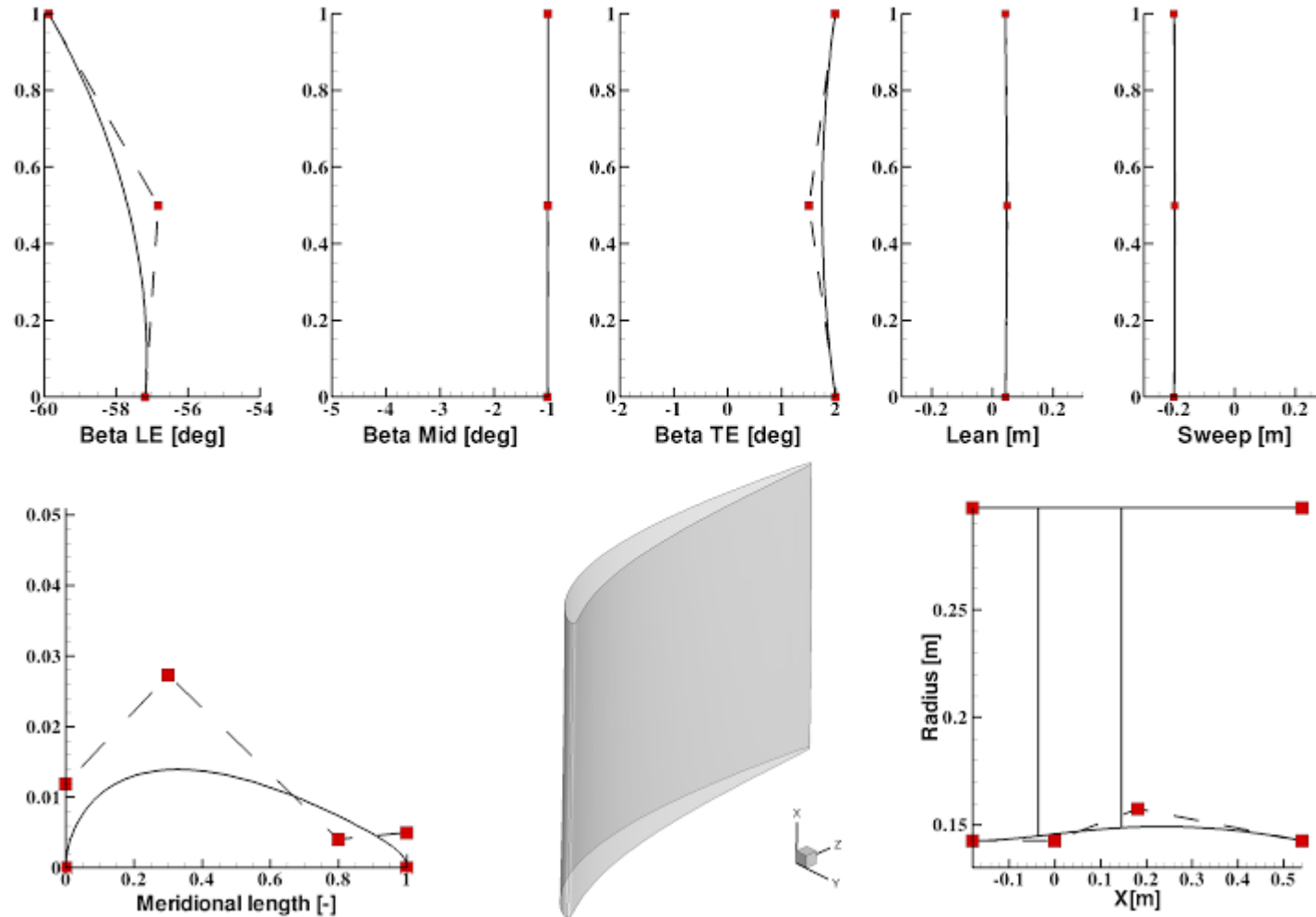
Optimization Results

$$\int_{hub}^{casing} \alpha_{whirl}^2$$

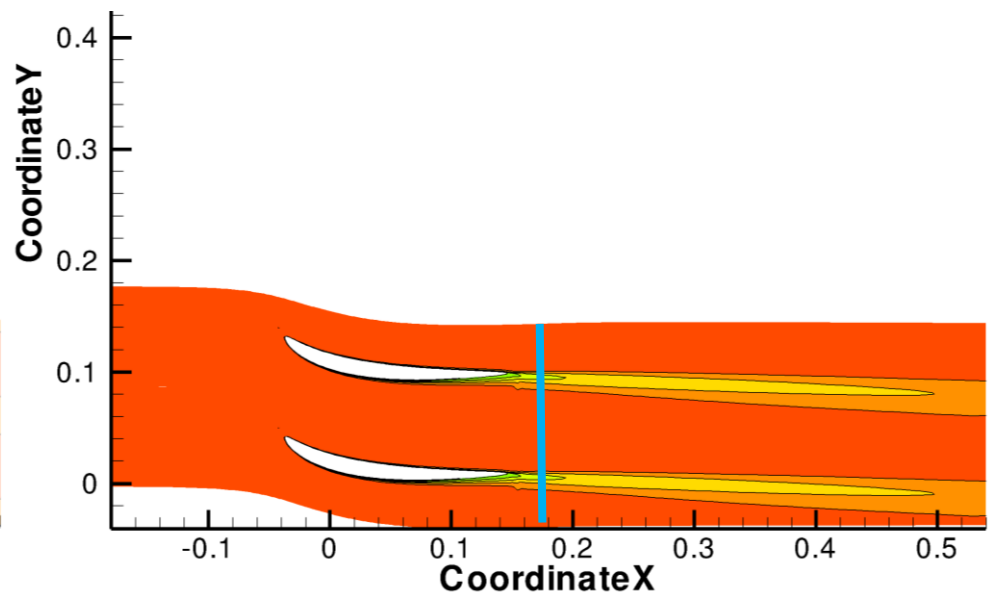
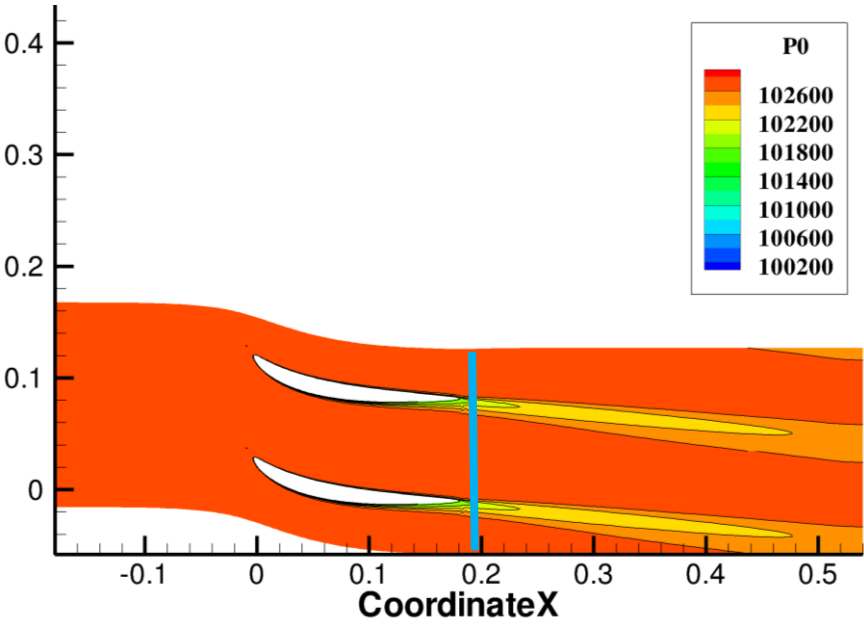
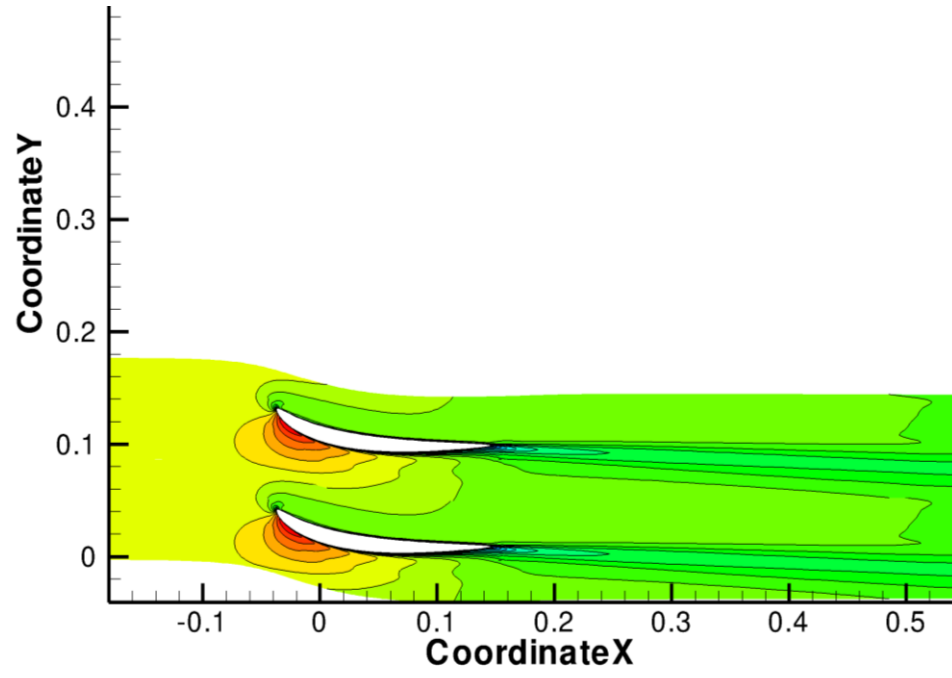
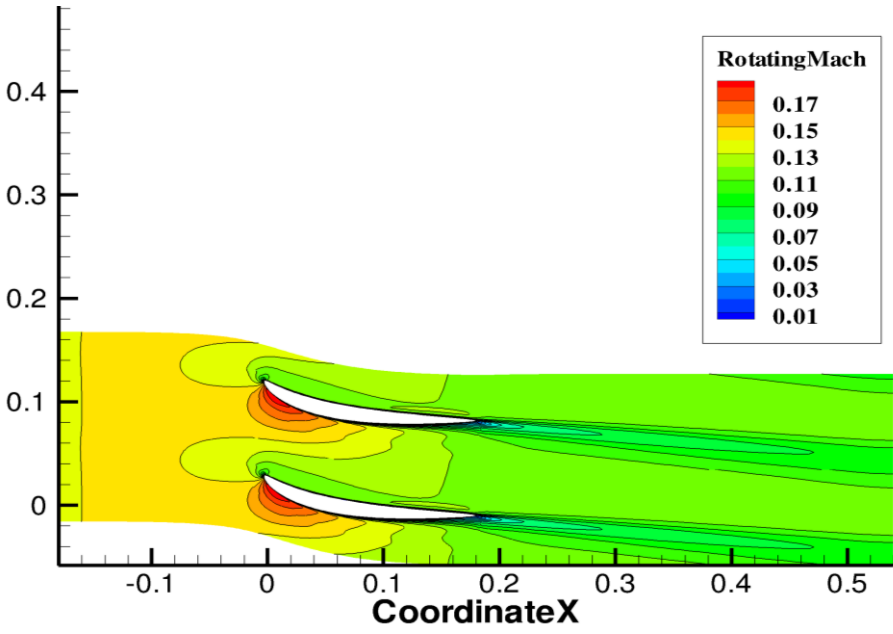


$$Loss_{P_0} = \frac{p_{01} - p_{02}}{p_{01} - p_1}$$

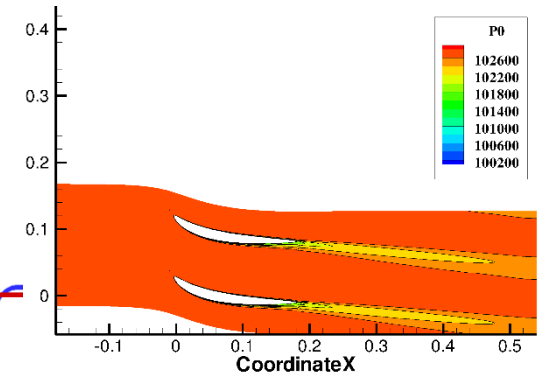
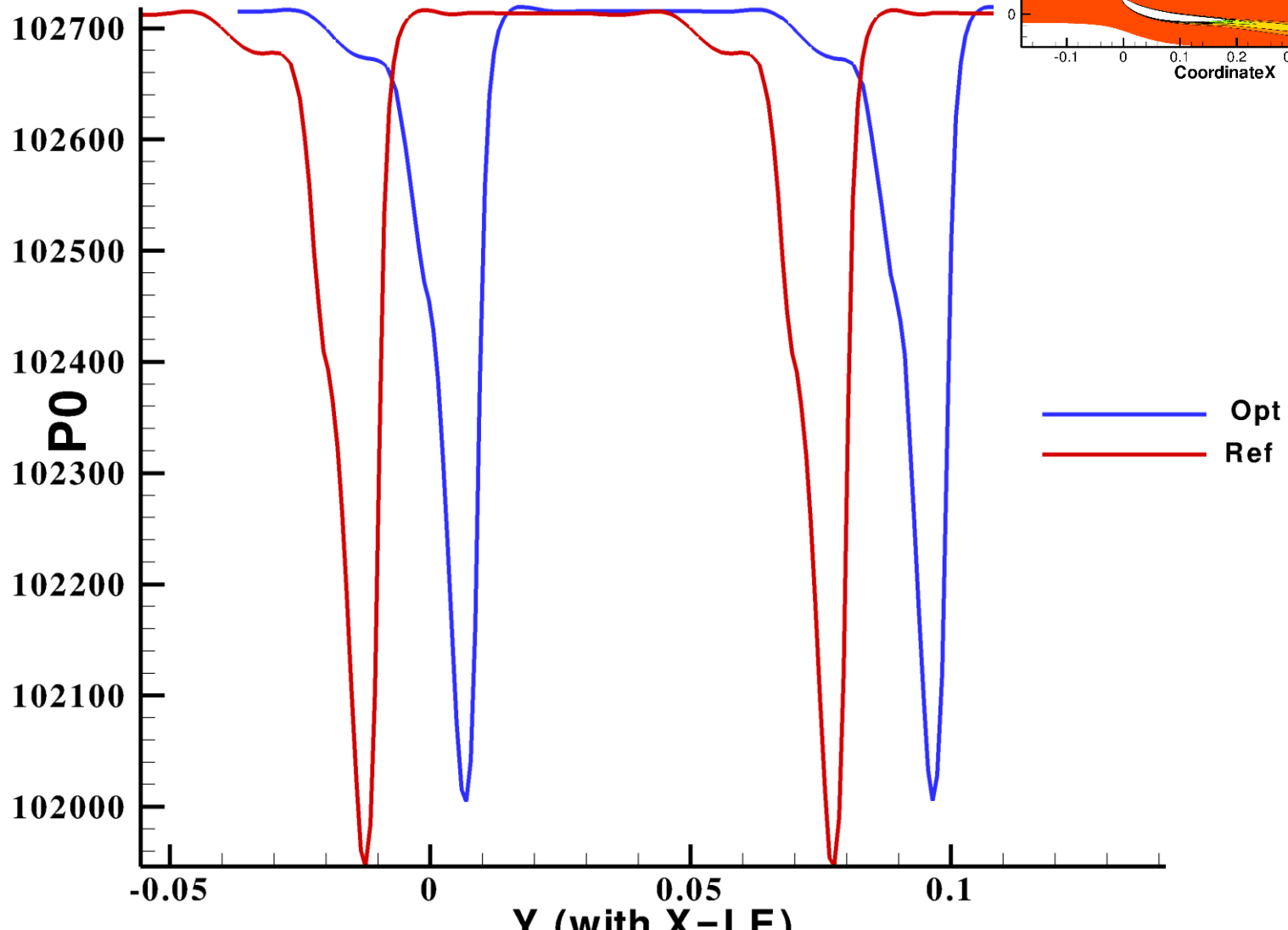
Optimized Blade



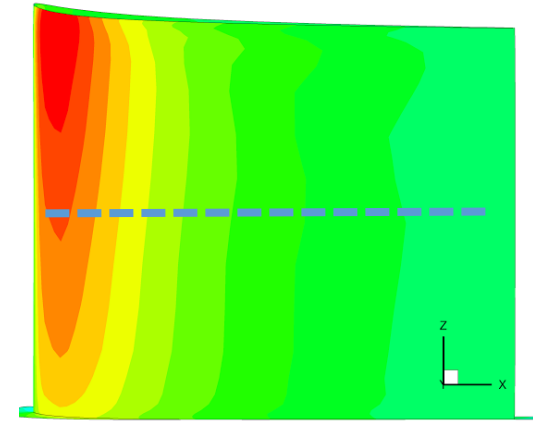
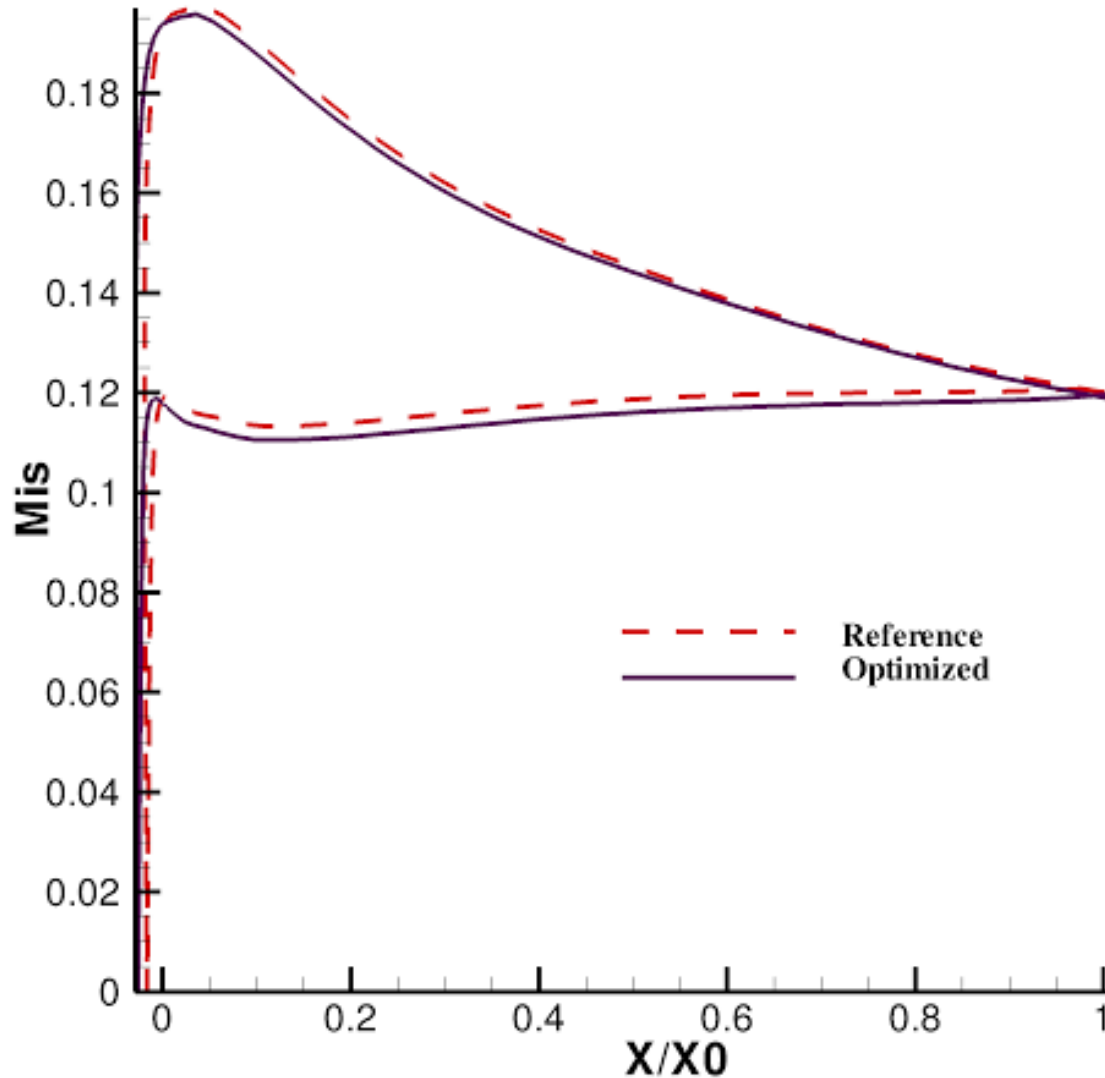
Baseline Vs Optimized



Baseline Vs Optimized



Isentropic Mach Number at mid-span

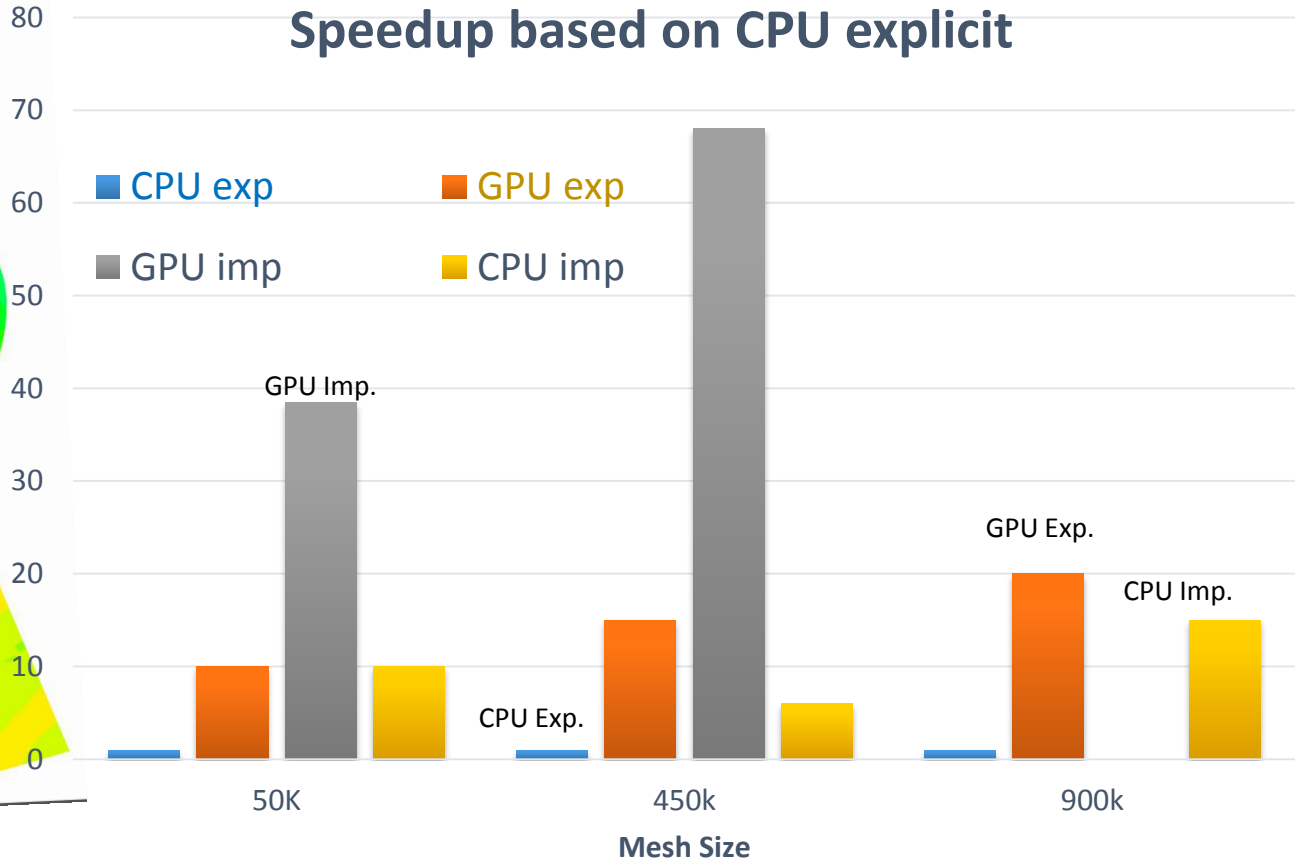
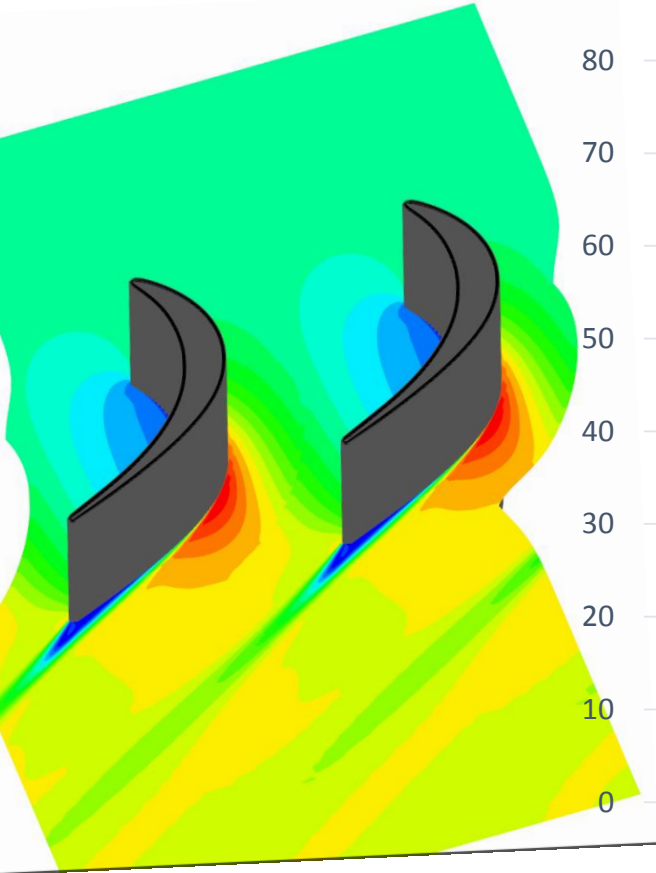


Conclusion

- Optimization
- GPU Solver with implicit time stepping
- *On-demand* (incomplete) Factorization
- 10x speedup
- Aerodynamic shape optimization

Future Work

Benchmark Case: Transonic Turbine Stator T106c



Thanks for your attention

Mohamed Hassanine Aissa

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acknowledgements:



Support



Hardware

